Coupled transport and population growth of *Pseudomonas putida* cells in the vicinity of a toluene source plume in a saturated sand-packed 2-D microcosm

A Dissertation

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### Abstract

Nearly half of all Americans drinking water comes from groundwater, while it suffers a great potential threat from the leakage of hazardous substances from underground storage tanks. According to US EPA, there are more than 400,000 confirmed underground storage tank leaks nationwide. Bioremediation is the treatment that uses naturally occurring microorganisms to break down these hazardous substances into less toxic or nontoxic substances. In the past years, increasing amount of data have been reported regarding the enhancement of the contaminant biodegradation rate by the chemotaxis of the microorganisms to these pollutants due to their increased delivery to the contaminated site, the process of which is often hindered by the non-uniform distributions of subterranean hydraulic conductivity. Although mixing transverse to the flow path is suggested to be a primary limiting factor for biodegradation efficiency, other steps can also contribute to the hindrance of the bioremediation process, for instance, the first step for the bacteria to degrade the contaminants is their uptake into the cell body. In this study, we investigated the impact of the toluene uptake step on the bioremediation efficiency using *Pseudomonas putida* F1 wild type and knockout mutant strains (PpF1 wild type, PpF1 ( $\Delta todX$ ), and PpF1 ( $\Delta todX\Delta cymD\Delta F1fadL$ )) whose toluene transmembrane transport channel(s) were removed, yet their chemotaxis to toluene was preserved. To this end, a bench-scale 2-D microcosm system was used as the study platform mimicking features of the naturally occurring groundwater system to study bioremediation efficiency limiting factors under conditions closer to those in natural aquifers. The application of mathematical models that incorporate the cell growth rate during this process - which is dependent on the toluene uptake that provides the cells with the carbon and energy source for survival and proliferation - will further elucidate to what extent the uptake step contributes to the bioremediation process in comparison with other steps such as dispersion and chemotaxis. The results revealed that PpF1 ( $\Delta todX$ ) that has reduced toluene transport capability, exhibited a lower percent recovery as compared with the wild type, implying less toluene consumption, and furthermore, exposure of the bacterial population to an increased toluene concentration (up to a certain level) increased the cell percent recovery. Furthermore, PpF1 ( $\Delta todX \Delta cymD \Delta F1 fadL$ )) that had even lower toluene uptake capability due to additional removal of toluene transport related channels, showed even lower recovery from the 2-D microcosm under the same experimental conditions. A mathematical model was then set up to study in detail the transport processes of the species during the microcosm experiments, and it was confirmed the sensitiveness of the toluene degradation efficiency to bacterial growthrelated parameters which was directly correlated with toluene uptake capability, regardless of the presence of mass transfer barrier. And this sensitiveness was reserved under different conditions, for example, in a region more distant to toluene source and at an increased flow rate which can occur at different geographic locations. This suggests that, in addition to mechanisms that enhance the delivery of the degrading agents to the contaminated site, transport membrane proteins of bacteria can also play a key role in bioremediation enhancement. Moreover, it suggests the potential of engineering bacteria toward higher contaminant permeability for enhanced bioremediation efficiencies.

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# List of Symbols

## Symbols

a	toluene concentration (chemoattractant)		
b	bacterial cell concentration		
0	oxygen concentration (electron acceptor)		
t	time		
Х	the distance longitudinally in the flow direction		
У	the transverse distance to the x axis		
$a_0$	injected toluene concentration		
$b_0$	injected bacterial concentration		
<b>O</b> <sub>0</sub>	injected oxygen concentration		
D <sub>a,bulk</sub>	bulk diffusion coefficient for toluene		
D <sub>a,eff</sub>	effective diffusion coefficient for toluene in porous media		
$D_{a,eff,ref}$	effective diffusion coefficient for toluene from reference		
$D_{ax}$	longitudinal dispersion coefficient for toluene		
D <sub>ax,ref</sub>	longitudinal dispersion coefficient for toluene from reference		
$D_{ay}$	transverse dispersion coefficient for toluene		
D <sub>ay,ref</sub>	transverse dispersion coefficient for toluene from reference		
D <sub>b,bulk</sub>	bulk diffusion coefficient for bacterial cell		
$D_{b,eff}$	effective diffusion coefficient for bacterial cell in porous media		
$D_{bx}$	longitudinal dispersion coefficient for bacterial cell		
$D_{by}$	transverse dispersion coefficient for bacterial cell		
D <sub>o,bulk</sub>	bulk diffusion coefficient for oxygen		
D <sub>o,eff</sub>	effective diffusion coefficient for oxygen in porous media		
$D_{ox}$	longitudinal dispersion coefficient for oxygen		
$D_{oy}$	transverse dispersion coefficient for oxygen		
K <sub>a</sub>	half saturation constant, growth on toluene		
K <sub>c</sub>	chemotaxis receptor binding constant		
K <sub>o</sub>	half saturation constant, growth on oxygen		
k <sub>decay</sub>	bacterial cell decay rate		
$MW_b$	molecular weight of bacterial cell		

MW <sub>o</sub>	molecular weight of oxygen		
MWt	molecular weight of toluene		
$q_a$	maximum reaction rate of toluene		
$q_o$	maximum reaction rate of oxygen		
R	retardation factor		
$v_b$	bacterial cell swimming speed		
$U_{\text{avg}}$	apparent flow rate		
$V_b$	single bacterial volume		
$V_f$	average interstitial velocity		
V <sub>f,hi</sub>	average interstitial velocity, high flow rate		
V <sub>f,ref</sub>	average interstitial velocity from reference		
$v_{set}$	bacterial cell settling velocity due to gravity		
$Y_{b/a}$	yield coefficient of the bacterial cell on toluene		
$Y_{b/o}$	yield coefficient of the bacterial cell on oxygen		

### **Greek letters**

$\alpha_{ax}$	longitudinal dispersivity for toluene	
$\alpha_{ay}$	transverse dispersivity for toluene	
$\alpha_{bx}$	longitudinal dispersivity for bacterial cell	
$\alpha_{by}$	transverse dispersivity for bacterial cell	
$\alpha_{ox}$	longitudinal dispersivity for oxygen	
$\alpha_{oy}$	transverse dispersivity for oxygen	
٤	porosity	
E <sub>ref</sub>	Porosity from reference	
$\sigma_b^2$	variance of bacterial concentration peak at microcosm outlet	
τ	tortuosity	
$\mu_{max}$	maximum specific growth rate of cell on toluene	
$\mu_{max,o}$	maximum specific growth rate of cell on oxygen	
$\chi_{0,eff}$	chemotactic sensitivity coefficient	

### **Chapter 1. Introduction**

With the rapid development of new technologies and industrialization of modern society, the production of pollutant substances places a large burden on the environment and is posing substantial risks for groundwater quality, due to the fact that many of these compounds are toxic, carcinogenic and teratogenic. When released as non-aqueous phase liquids (NAPL), large amounts of contaminants can be trapped in soils and remain there until they slowly dissolve into groundwater, a process that can continue for decades or even centuries (1-8). According to a study by European Soil Data Centre of the European Commission, the number of estimated potential contaminated sites is more than 2.5 million and the identified contaminants contributing around 60% to soil contamination (2). In the US, approximately 558,000 underground storage tanks nationwide store petroleum or hazardous substances, and there are more than 400,000 confirmed underground storage tank leaks nationwide (3-4).

Aromatic hydrocarbons are widespread pollutants within the environment owing to natural releases, improper industrial and social activities, such as the widespread occurrences of leakage from underground petroleum storage tanks and spills at petroleum production wells and refineries, and their removal has proven to be very challenging. As a result, aromatic hydrocarbons are listed as priority pollutants by the US Environmental Protection Agency (9). In addition, due to the limited chemical reactivity and hydrophobic character, aromatic hydrocarbons and many other xenobiotics are highly persistent within the environment. Besides the obvious health-related factors, there is also a considerable economic burden resulting from the presence of pollutants within the environment due to the high costs of the treatment and cleanup of contaminated sites by various abiotic methods, such as incineration of soils, soil washing, pump and treat, *etc*. (10-18).

Moving together with the groundwater flow, the dissolution of aromatic hydrocarbon contaminants into the groundwater forms a contaminant plume. The lengths of contaminant plumes vary between several to a few hundred meters and the total expanse is specifically governed by natural attenuation. Most abiotic attenuation process, for example, dilution, sorption, ion exchange, volatilization, precipitation, chemical transformation and dispersion (19-22), only play a role during the early stages of contamination until microbial degradation becomes established. Subsequently, microbial activity is the only process that effectively leads to a net loss of pollutants in plumes contaminated with petroleum hydrocarbons (23-32). Thus, there has been a great amount of interest concerning metabolism of pollutants by bacteria as well as the application of those bacteria for the removal of xenobiotics from the environment (23-34). In situ bioremediation has been demonstrated to be an efficient and cost-effective method to reduce organic contamination under certain conditions (14, 33-37). Compared with the traditional pump-and-treat approach, it mainly utilizes bacteria, by either stimulating indigenous species (biostimulation) or introducing exogenous species (bioaugmentation), to metabolically degrade the contaminants without disturbing the natural environment or requiring large space for equipment.

Bioremediation is a complex process involving a series of steps including the delivery of the biodegraders to the contaminants, the contaminant uptake and the metabolism of the contaminants by the biodegraders. Experimental studies by Griebler and coworkers (38-40) showed that biodegradation occurred at the edges of contaminant plumes and was mixing-controlled; however, under different conditions other steps may be the limiting

factors, for example, the passage of hydrophobic substrates into the cell body, in regard to the effective barrier of the cells against alien molecules. In this study, we propose to investigate the impact of this uptake step on bioremediation, comparing strains that differ in their permeability to the contaminants under conditions that are relevant for the natural environment. The application of a mathematical model that accounts for transport, proliferation and degradation will quantify the extent to which the bioremediation is dependent on the uptake step as compared with the delivery of cells to the contaminated site. To this end, a model system comprising of the degraders *Pseudomonas putida* FIstrains and the contaminant toluene was used where a saturated sand packed 2-D microcosm served as the study platform.

*Pseudomonas putida F1* (PpF1) has a number of advantages, which make it an ideal model microorganism for this study. PpF1 is known to be chemotactic to a number of aromatic hydrocarbons and chlorinated aliphatic compounds, a property that is likely to aid its efficiency as a biodegrader (41). While many bacterial isolates have been identified with aromatic hydrocarbon-degrading capabilities, only few of them have been characterized in detail. PpF1 was isolated from a polluted creek in Urbana (IL), and was the first biodegrader whose genome was sequenced (42). It has a large genome of 6.0 Mb and is a versatile organism found in soil and water that is capable of growth on the mono-aromatic hydrocarbons (MAH) benzene, toluene, ethylbenzene and p-cymene (43).

To test the toluene uptake step on bioremediation efficiency, PpF1 mutant strains were generated by knocking out the uptake channels, which led to impaired uptake capability comparing with the wild type. PpF1 is a gram-negative bacterium where the thin peptidoglycan layer of their cell wall is sandwiched between an inner cytoplasmic cell membrane and a bacterial outer membrane. The outer membrane of PpF1 is a very effective barrier against the permeation of hydrophobics such as toluene, due to the lipopolysaccharide in the outer leaflet of the outer membrane. Thus, the outer membrane is a unique lipid bilayer that requires specific channels for the uptake of hydrophobics such as aromatic hydrocarbons destined for biodegradation and these specific channels are usually trans-membrane proteins encoded by the bacterial genome. Besides the availability of the genomic sequence, another advantage of PpF1 is that all its biodegradative capabilities are encoded on the chromosome and not on a large catabolic plasmid, as is the case for many biodegrader strains. This removes the need to ensure that the plasmid is maintained and avoids potential incompatibilities with expression plasmids used for gene complementation.



**Figure 1.1** The *tod* operon controls toluene degradation in *Pseudomonas putida* F1. Toluene (A) is catalyzed by a series of enzymes in the *tod* operon to 2-hydroxy-6-oxo-2, 4-heptadienoate (B) and then 2-hydroxypenta-2, 4-dienoate (C) before entering the TCA cycle to produce  $CO_2$  and  $H_2O$ . *todX* is believed to be the gene for the transport channel on the bacteria membrane to uptake toluene. Operon *cymD* is also confirmed to support the growth of *Pseudomonas putida* F1 on toluene by van den Berg lab although the exact metabolic pathway has not been fully elucidated yet.

PpF1 has two operons responsible for the degradation of MAH, located adjacent to each other. These operons are designated *tod* (toluene degradation) and *cym/cmt* (p-cymene/p-cumate). The *tod* operon (**Figure 2.1**) consists of the genes *todXFC1C2BADEGIH*, which together encode for seven enzymatic reactions. All enzymes within the *tod* operons are soluble and located within the cytoplasmic space. The operon contains one member of the

FadL family of outer membrane channels, TodX. While the involvement of TodX in substrate uptake in PpF1 has not been demonstrated, there is inconclusive experimental evidence linking the FadL orthologs TbuX to toluene uptake in *Ralstonia pickettii* and XylN to toluene uptake in *Pseudomonas putida* F1 (44). A *tod* knockout strain and a *tod/cymD/FadL* triple knockout strain were generated by the van den Berg lab (Newcastle University, UK), which demonstrated decreased toluene permeability as compared with wild type. Furthermore, TodX is known to not affect the PpF1 chemotactic pathway (39).

The objective of this study is to investigate the impact of contaminant uptake by microorganisms on bioremediation with a bench-scale 2-D microcosm under conditions that are relevant for the natural environment, where mass transfer limitations have posed a significant barrier for bioremediation efficiency. Bioremediation being a complex process comprises a series of steps, i.e., the delivery of the biodegraders to the contaminants, the uptake of the contaminant, and the chemical transformation of the contaminants by the biodegraders. While previous studies emphasized mass transfer as the limiting factor for the overall rate of contaminant removal, the subsequent uptake step can also contribute to the remediation efficiency. This study will not only be of fundamental importance in clarifying the mechanisms underlying the bioremediation processes, but also in providing insights that lead to the design of bacterial strains with altered and/or enhanced biodegradation properties.

In this study, it is hypothesized that in a 2-D microcosm mimicking features of the natural groundwater system, the toluene uptake can serve as the "remediation-rate-liming" step. Thus, it is expected that the PpF1 cell strain with the greater toluene uptake rate proliferates faster upon the consumption of toluene as sole carbon source inside the microcosm in comparison to the strain with the lower toluene uptake rate. To test this

hypothesis, a 2-D microcosm mimicking the natural groundwater system will be used as the study platform wherein both mass transfer and toluene uptake can play a role in the proliferation rate. First, PpF1 wild type and PpF1 ( $\Delta todX$ ) strains will be respectively introduced above and below the toluene plume during the same microcosm run. As they travel through the microcosm from one end to the other, transverse dispersion as well as chemotaxis serve as transport mechanisms that bring them closer to the toluene plume upon which they survive and proliferate. PpF1 ( $\Delta todX$ ) strain whose toluene uptake channel has been knocked out are expected to proliferate to a lesser extent than the wild type. Next, a triple knockout mutant strain PpF1 ( $\Delta todX$ ,  $\Delta cymD$ ,  $\Delta FadL$ ) with even lower toluene uptake capability, whose proliferation rate is expected to be even slower. will be tested in the same way. Furthermore, a mathematical model quantifying transport, uptake and degradation will be set up and matched to the experimental system to evaluate in detail how and how much the chemotactic and cell growth/death parameters affect the overall bioremediation process. Under natural environment, typical groundwater flow rate in a sandy or gravelly aquifer may range from 0.5 to 50 feet per day (45, 46), and the location where the biodegraders are delivered to in regard to the contaminant source also varies case by case. These are factors that can affect the portion of the contributions of different steps during the remediation process. Thus, the mathematical model was also tested at a higher flow rate as well as a longer spacing distance between the toluene and the biodegrader injection ports, and the effect of chemotaxis and contaminant uptake rate on bioremediation process were compared under such conditions.

### **Chapter 2. 2-D Microcosm Experiments**

### 2.1. Introduction

An overview of this chapter is presented below. Three PpF1 strains are used in this study: *Pseudomonas putida* F1 wild type (PpF1 wild type) which has full capability of toluene uptake, *Pseudomonas putida* F1 single knockout strain (PpF1 ( $\Delta todX$ )) which has impaired toluene uptake capability, and *Pseudomonas putida* F1 triple knockout strain (PpF1 ( $\Delta todX\Delta cymD\Delta F1fadL$ )), which has even higher degree of impaired toluene uptake capability. The wild type strain and two mutant strains were obtained from Bert van den Berg lab (Newcastle University, UK).

Before 2-D microcosm experiments were performed, growth of three types of PpF1 strains were compared both by culture on LR agar plate and by culture in LR liquid media where the toluene as the sole carbon source was supplied in the gas phase. Details were presented in Chapter 2.2.

In Chapter 2.4, 2-D microcosm experiments were first conducted in the absence of a toluene plume to establish the baseline migration behavior for the PpF1 wild type and PpF1 single knockout strains. In Chapter 2.5, subsequent 2-D microcosm experiments in the presence of toluene were designed for PpF1 wild type and PpF1 single knockout strains to test their response to low and high concentration of toluene. Lastly in Chapter 2.6, a new set of 2-D microcosm experiments were carried out for PpF1 triple knockout strain, following the same experimental design for PpF1 single knockout strain, to assess how different toluene uptake capability affect the PpF1 population growth and migration.

Table 2.1.1 Thr	ee types of PpF1	strains and	genotype.
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Strain genotype	Strain characteristic	Strain label
PpF1 wild type	PpF1 wild type	PpF1 f0
PpF1 ( <i>∆todX</i> )	PpF1 single knockout strain	PpF1 f1
PpF1 ( <i>∆todX∆cymD∆F1fadL</i> )	PpF1 triple knockout strain	PpF1 f3

#### 2.2. Materials and methods

Growth of three types of PpF1 strains were compared both by culture on LR agar plate and by culture in LR liquid media where the toluene as the sole carbon source was supplied in the gas phase.

Growth rates of three PpF1 strains were compared by culture on an LR agar plate (prepared as described in **Appendix A6**) where toluene as the sole carbon source was supplied in the gas phase. A single colony of PpF1 wild type, PpF1 single knockout strain or PpF1 triple knockout strain was picked from an LB plate that had been stored in 4 °C then inoculated to 3 mL LB media in a tube. PpF1 cells were cultured in a shaking incubator overnight with a rotation rate of 150 rpm at 28 °C. The cells were harvested by centrifugation at 4,000 xg for 10 min and washed with autoclaved H<sub>2</sub>O then harvested again. This washing step was repeated one more time. Then PpF1 cell concentration was adjusted to OD<sub>590</sub>=1 with autoclaved H<sub>2</sub>O. 5 uL of this cell suspension was dropped on an LR agar plate and streaked with an autoclaved inoculating loop. The inoculated LR plate was put in a sealed container wherein 50 uL of toluene was supplied in a 1.5 mL closed-cap microcentrifuge tube and incubated at 30 °C for 2 days before photos were taken. The microcentrifuge containing toluene was replaced every day.

Growth rates of three PpF1 strains were also tested by culture in liquid media for a more quantitative comparison than the visual observation on agar plate. PpF1 cells were first activated in LB media through tube culture then washed as mentioned above. Equal amounts of three types of PpF1 cells were inoculated separately to each autoclaved 100 mL duran bottle containing 25 mL LR liquid medium and 1 uL or 2 uL of toluene supplemented in an open-cap microcentrifuge tube, and cultured at a rotation rate of 180 rpm at 23-25 °C. Cell concentration was measured at wavelength of 590 nm after 16 h of

culture.

To prepare cells for 2-D microcosm experiments, a single colony of each PpF1 strain was picked from an LB agar plate that had been stored in 4 °C and inoculated into 3 mL LB liquid media in a tube. PpF1 cells were cultured in a shaking incubator overnight at a rotation rate of 150 rpm at 28 °C. Equal portions of each strain were then inoculated separately into 250 mL flasks containing 50 mL of growth media supplemented with toluene and cultured for 9 h under at a rotation rate of 150 rpm at room temperature. Then, cells were harvested by centrifugation at 4,000 xg for 10 min and washed with autoclaved deionized H<sub>2</sub>O. This washing step was repeated one more time. Cell concentration was adjusted to  $OD_{590}$ = 0.5-1 with autoclaved running buffer that was used within the 2-D microcosm.





12 ea outlet

Figure 2.2.1 A 2-D microcosm was used in this study to mimic the natural groundwater system.

The 2-D microcosm experimental setup is shown in **Figure 2.2.1** (5). The 2-D microcosm mimics the contaminated groundwater system with water flowing steadily through the saturated sand-filled tank from one end to the other. The toluene plume is marked by co-

injection of a color indicator resazurin that appears purple and the PpF1 cell plumes are visible by co-injection with uranine, which appears yellow.

The 2-d microcosm had a Teflon base, Teflon end pieces, an aluminum frame, and two sheets of glass all sealed watertight with silicone glue wherein Ottawa sand was packed. The inner dimensions measured 95 cm x 14 cm x 1 cm and the apparatus sat on two wooden supports with a spill tray underneath. The inlet and outlet ends of the 2-D microcosm were equipped with twelve ports with a vertical spacing of 1 cm numbered 1 through 12 from top to bottom. Two-inch long stainless steel capillaries were fitted through the ports. The inflow and outflow capillaries extended 0.5 cm into the microcosm. The outflow capillaries were wrapped with 1 cm x 1 cm piece of steel woven wire fine mesh to the prevent sediment from clogging the capillaries. The outer capillary tips were connected to PVC pump tubing links (PVC solvent/hydrocarbon tubing, twostop, 0.89 mm ID), which ran through two twelve-channel Carter peristaltic precision pumps (Manostat Carter, Thermo Scientific), one for the inflow and another for the outflow. The pump was calibrated prior to each run so that the flow rate variance from each channel was less than 5%. The inlet ports were used to transfer the running buffer M9 media (47) from a 1L storage bottle into the microcosm. The effluent media pumped from the outlet ports was directed into the sample collection containers during sample collection period and otherwise to a hazardous waste collection container. The flow rate is controlled by both inflow and outflow pumps.

Prior to each experiment, the microcosm tank was rinsed with 0.3 M NaOH solution followed by autoclaved  $H_2O$  three times and then a last washing step with autoclaved M9 media. Before injection of any solution into the sand-packed microcosm, M9 medium was pumped through for at least 12 h to reach a steady flow, during which a stable water table was established below

a thin unsaturated layer on top of the microcosm. The flow rate was about  $1.1 \sim 1.3$  m/d, which is similar to the natural groundwater velocities (33).

In general, the PpF1 cell suspension and attractant solution will be continuously fed at different vertical locations. In this experiment, when two PpF1 cells were injected into the microcosm, port 7 was dedicated for M9 containing toluene and uranine, and port 4 and port 10 for different PpF1 strains. After traveling through the microcosm, various samples containing uranine, resazurin, resorufin, toluene, and PpF1 cells at the outlet were collected over a range of vertical positions for 2 h and their concentration distribution was analyzed by various analytical methods, which are detailed in the Appendices.

### 2.3. Comparison of cell growth

#### 2.3.1. Comparison of cell growth on agar plate

As **Figure 2.3.1** shows, under the same culture condition, the PpF1 wild type exhibited greater growth rate than two PpF1 knockout strains, and PpF1 single knockout strain grew slightly faster than PpF1 triple knockout strain. Notice that both of the two knockout strains also had a slight growth in spite of the absence of the toluene-specific transport channels. According to van den Berg lab (Newcastle University, UK), this is due to leakage of toluene transport across the membrane via other pathways.



**Figure 2.3.1** Comparison of growth of three PpF1 strains on LR agar plate where toluene was supplied in the gas phase. 1: PpF1 wild type; 2: PpF1 single knockout strain; 3: PpF1 triple knockout strain. The growth rate is in the order: PpF1 wild type > PpF1 single knockout strain > PpF1 triple knockout strain.

### 2.3.2. Comparison of cell growth in liquid media

For a more quantitative growth comparison than the visual observation on agar plate, growth rates of three PpF1 strains were also tested by culture in liquid media. Similar to the result from growth comparison on agar plate, in liquid media as well, the PpF1 wild type proliferated fastest, PpF1 triple knockout strain slowest, and PpF1 single knockout strain in between (**Table 2.3.1** and **Table 2.3.2**, **Figure 2.3.2**). Regardless of the lack of a certain trans-membrane toluene transport proteins, PpF1 knockout strains still showed a certain level of growth, implying that there are other pathways for toluene to be uptake by PpF1 cells.

				-	-								
Strain	#	Toluene	<b>OD</b> <sub>590</sub>	Avr.	SD	CV	Strain	#	Toluene	<b>OD</b> <sub>590</sub>	Avr.	SD	CV
	f0-1	1 uL	0.113	0.097	0.011	12%		f0-1	2 uL	0.159	0.179	0.020	11%
PpF1	f0-2	1 uL	0.091				PpF1	f0-2	2 uL	0.164			
wild type	f0-3	1 uL	0.097				wild type	f0-3	2 uL	0.192			
	f0-4	1 uL	0.087					f0-4	2 uL	0.2			
DnE1	f1-1	1 uL	0.055	0.070	0.017	24%	DnE1	f1-1	2 uL	0.076	0.090	0.015	16%
cipalo	f1-2	1 uL	0.056				single	f1-2	2 uL	0.079			
single	f1-3	1 uL	0.087				knockout	f1-3	2 uL	0.101			
KHOCKOUL	f1-4	1 uL	0.081				KHOCKOUL	f1-4	2 uL	0.105			
DraE4	f3-1	1 uL	0.025	0.029	0.007	25%	PpF1	f3-1	2 uL	0.047	0.045	0.024	53%
PPF1	f3-2	1 uL	0.021				triple	f3-2	2 uL	0.02			
unple	f3-3	1 uL	0.036				knockout	f3-3	2 uL	0.068			
KHOCKOUT	f3-4	1 uL	0.035										

**Table 2.3.2.1** Cell density of three PpF1 strains measured after 16-hour culture in LR media with toluene supplied at gas phase

 Table 2.3.2.2 Statistical analysis of growth rates of three PpF1 strains

	<i>p</i> -value			
	Toluene 1 uL	Toluene 2 uL		
PpF1 wild type vs PpF1 single knockout	0.03560	0.000411		
PpF1 wild type vs PpF1 triple knockout	0.00006	0.000491		
PpF1 single knockout vs PpF1 triple knockout	0.00435	0.026710		



**Figure 2.3.2.1** Comparison of growth of three PpF1 strains in liquid media. The growth rate is in the orde: PpF1 wild type > PpF1 single knockout strain > PpF1 triple knockout strain. The growth rates of three PpF1 strains are statistically significant (*p*-value <0.05).

#### 2.4. 2-D microcosm experiments: without toluene

2-D Microcosm experiments were first conducted in the absence of a toluene plume to establish the baseline migration behavior for the wild type and PpF1 single knockout strains. Each PpF1 cell suspension was fed continuously from an inlet port, and it was transported along with the continuous convective flow toward the outlet. Dispersion contributed to the spread of the plume vertical to the flow direction, such that the concentration yielded a Gaussian-shaped distribution at the outlet. Characterization of PpF1 cell distributions in the effluent was done with Gaussian fitting (details in the **Appendix A5**). The schemes and pictures of actual 2-D microcosm runs with PpF1 wild type and PpF1 single knockout strains are shown below.

In **Figure 2.4.2**, the distributions of PpF1 wild type and PpF1 single knockout strains are plotted side-by side for comparison. Uranine was co-injected with the bacteria as an internal control for the fluid flow behavior in the microcosm. The vertical position of the bacterial profiles was thus plotted relative to the uranine position for that particular experimental run to compensate for small variations in the fluid velocity between different microcosm trials. The uranine and PpF1 cell distribution profiles were subjected to Gaussian fitting (**Appendix A5**) to determine the peak center as well as the breadth of each peak. The peak center is indicated by the mean and the peak breadth by variance  $\sigma^2$  Fitting result is shown in **Table 2.4.1**. Comparing the center of mass relative to the uranine tracer, both PpF1 strains settled downward from the injection altitude, as their specific gravity was greater than unity. The settling velocity of both PpF1 strains appeared to be comparable as the center of mass shifted downward by about 1 cm for each strain.



Figure 2.4.1 Schemes and pictures of 2-D microcosm runs without toluene.



**Figure 2.4.2** Concentration profiles of two bacterial strains, PpF1 wild type (PpF1 f0) and PpF1 single knockout strain (PpF1 f1) at the 2-D microcosm outlet. Uranine served as a tracer and internal control.

**Table 2.4.1** Comparison of parameter values (mean  $\mu$  and variance  $\sigma^2$ ) from Gaussian fitting of uranine tracer concentration and bacterial cell counts in 2-D microcosm effluent samples for PpF1 wild type and PpF1 single knockout strain.

	PpF1 wild	type	PpF1 single knockout			
	Uranine	Cell	Uranine	Cell		
μ (cm)	0	-0.9	0	-1.1		
$\sigma^2$ (cm <sup>2</sup> )	2.0	0.7	1.8	0.8		
Transverse dispersivity (cm)	0.0053	0.0018	0.0043	0.0022		

A force balance on the cell accounting for Stokes drag yields  $v_{settling} = \frac{(\rho_P - \rho)gd_P^2}{18\mu}$ ,

where  $v_{settling}$  is the theoretical settling velocity for a perfect sphere,  $\rho_P$  and  $d_P$  are the respective buoyant density and diameter of the particle,  $\rho$  is the fluid density, and  $\mu$  is the dynamic fluid viscosity, and g is the acceleration due to gravity (48). Estimating  $\rho_P$ = 1.11e3 kg/m<sup>3</sup>,  $\rho$ = 1e3 kg/m<sup>3</sup>, g= 9.8 m/s<sup>2</sup>,  $d_P$ = 1e-6 m, and  $\mu$ = 1e-3 kg·m<sup>-1</sup>s<sup>-1</sup> (49), the calculated settling velocity is  $v_{settling}$  =6.0e-8 m/s. Thus, over the averaged traveling time of 20 h, the settling distance is 0.39 cm, which is the same order of magnitude as the observed value 1 cm. The difference between the estimated and observed settling distances may be attributed to the idealized spherical shape as well as an underestimate of the cell diameter and the cell density that were used in the calculation.

Uranine recovery in the runs for PpF1 wild type and PpF1 single knockout strain were 39.8% and 58.3%, respectively, and the cell recovery after calibration by uranine yielded 391% and 355% for each of them.

Dispersivity was calculated as follows:

From the Einstein relationship,  $D_T = \frac{\sigma^2}{2t}$ , where  $D_T$  is the transverse diffusion coefficient,  $\sigma^2$  is the second moment and t is the traveling time.

 $D_T = \frac{D_{eff}}{\varepsilon} + \alpha_T v$ , where  $D_{eff}$  if the effective diffusion coefficient,  $\alpha_T$  is the dispersivity and v is the swimming speed. So,  $\alpha_T = \frac{(\frac{\sigma^2}{2t} - \frac{D_{eff}}{\varepsilon})}{v}$ , where t= 19 h, v = 1.55 e-5 m/s,  $\varepsilon = 0.37$ ,  $D_{eff}$  for uranine is 9.0e-6 cm<sup>2</sup>/s and  $D_{eff}$  for a cell is 3.2 e-6 cm<sup>2</sup>/s. The transverse dispersivity for each analyte in each run is listed in **Table 6.1.1**.

These values are similar in magnitude to previously reported values of 0.0005-0.0012 cm for *E. coli* bacteria (31) and 0.004-0.010 for small molecules (38, 31, 32) from other microcosm set-ups and a smaller-scale microfluidics device. The vertical spread of both cell types as measured by the second moment was comparable to each other, and less than that of uranine. This is likely due to the larger size of cells than uranine molecules where the larger particles make less detours in transverse direction as they flow along with the streamlines (31, 50). The results from the moment analysis show the knockout of TodX from PpF1 doesn't have a significant effect on the cell transport during the microcosm run.

#### 2.5. 2-D Microcosm experiments: low & high concentration of toluene

With toluene fed into the 2-D microcosm, two experimental configurations with two different toluene concentrations were studied as shown in **Figure 2.5.1** (Actual images in **Appendix A7.1** and **A7.2**). The lower concentration of toluene (1e-5 v/v) was fed for Run 1 and Run 2, and the higher concentration of toluene (1e-4 v/v) was fed for Run 3 and Run 4. For the same feed concentration of toluene, two different PpF1 strains - PpF1 wild type and PpF1 single knockout strain - were injected, with one above and the other below the toluene plume during the same run. Also a run where the positions were switched was also tested.

PpF1 strains were injected in a suspension without a carbon source. As cells moved horizontally together with the convective flow of buffer, dispersion as well as chemotaxis and settling due to gravity drove the vertical movement of cells toward or away from the toluene plume. Upon exposure to toluene, which serves as the sole carbon source for PpF1 cell survival and proliferation, the population growth of PpF1 single knockout strain was observed to be less than PpF1 wild type, due to the impaired toluene uptake capability.

To compare the difference of PpF1 wild type and PpF1 single knockout strain in growth rate, the percent recovery of cells at the effluent was analyzed and the results are listed in **Table 2.5.1**. Cell recovery was calibrated relative to the uranine recovery that was co-injected together with the cells. **Figure 2.5.2** shows a representative concentration profile of cell and uranine concentrations at the outlet using Run 3 as an example (others are in **Appendix A7.1** and **A7.2**). The area under each peak represents the quantity recovered of the corresponding analyte.


**Figure 2.5.1** Configurations for four different microcosm runs with PpF1 wild type (PpF1 f0) and PpF1 single knockout strain (PpF1 f1).



**Figure 2.5.2** Concentration profiles of cells and uranine for microcosm Run 3. PpF1 wild type (PpF1 f0) was injected above the toluene plume and PpF1 single knockout strain (PpF1 f1) below the toluene plume.

**Table 2.5.1** List of cell recovery data in four microcosm runs. The same shading/patterning represents the same microcosm run, respectively. At the outlet of each microcosm run, cells were collected, counted, and calibrated to uranine recovery, then compared with the inlet concentration for the percent recovery calculation.

PnF1 strain	Injection location	<u>% Recovery</u>		
PPFI Strain	Above/Below toluene plume	1e-5 v/v	1e-4 v/v	
PpE1 wild type	Above (top)	170%	431%	
FPF1 wild type	Below (bottom)	232%	219%	
PpE1 single knockout strain	Above (top)	86%	124%	
	Below (bottom)	127%	213%	



**Figure 2.5.3** Plot of cell recovery for PpF1 wild type and PpF1 single knockout strain when injected above and below the toluene plume, both at low and high concentration of toluene.

In each microcosm run, PpF1 wild type recovery was greater than PpF1 single knockout strain: 170% vs. 127%, 232% vs. 86%, 431% vs. 213%, and 219% vs. 124% (**Table 2.5.1**). These results were as expected: the lack of TodX led to less uptake of toluene by the PpF1 single knockout strain (PpF1 ( $\Delta todX$ )) and consequently reduced population growth.

In comparing microcosm runs with low and high toluene concentration feed it was noted that: PpF1 wild type had higher recovery at higher toluene concentration, 431% vs. 170% when injected above the toluene plume; and a comparable percent recovery at high and low toluene concentration, 219% vs. 232% when injected below the toluene plume.

PpF1 single knockout strain had higher recovery at high toluene concentration 124% vs. 86% when injected above the toluene plume; and higher recovery at low toluene concentration 219% vs. 127% when injected below the toluene plume.

Overall, it was revealed that under the current experimental conditions mimicking the natural groundwater environment, PpF1 single knockout strain achieved lower population growth as compared with the wild type, and exposure of the PpF1 cells to a certain level of increased toluene concentration accelerated the cell population growth. It implies that the toluene uptake step can play an important role in bioremediation enhancement and also suggested the potential of engineering bacteria toward higher contaminant permeability for enhanced bioremediation efficiencies.

# 2.6. 2-D Microcosm experiments: three PpF1 strains

With PpF1 single knockout strain grew slower than PpF1 wild type in the microcosm when toluene served as the only carbon source over the run, the same set of experiments were conducted for another strain PpF1 triple knockout mutant, with exactly the same setting as 2-D microcosm runs with PpF1 single knockout strain which had more toluene uptake related transport proteins knocked out thus showed even lower growth rate on agar plate as well as in liquid media. The scheme was drawn in **Figure 2.6.1** and cell recovery at the 2-D microcosm outlets was measured and adjusted over the uranine recovery at the end of the experiments (concentration profiles in **Appendix A7**). The corresponding graph comparing cell recovery of three PpF1 strains was shown in **Figure 2.6.2**.

With 1e-4 v/v toluene supply, when PpF1 strains were injected above the toluene plume, the cell recovery was in order of PpF1 wild type > PpF1 single knockout strain > PpF1 triple knockout strain. With 1e-4 v/v toluene supply, when PpF1 strains were injected below the toluene plume, the cell recovery was in order of PpF1 wild type  $\approx$  PpF1 single knockout strain > PpF1 triple knockout strain. This is the same order as toluene uptake capability of three PpF1 strains, indicating that with the mass transfer barrier existing inside the microcosm, toluene uptake capability of PpF1 strains still played a dominant role in degrading toluene.



**Figure 2.6.1** Configurations for two different microcosm runs with PpF1 wild type (PpF1 f0) and PpF1 triple knockout strain (PpF1 f3).

**Table 2.6.1** List of cell recovery data for three PpF1 strains during 2-D microcosm experiments with 1e-4 v/v toluene fed: PpF1 wild type (PpF1 f0), PpF1 single knockout strain (PpF1 f1) and PpF1 triple knockout strain (PpF1 f3). At the outlet of each microcosm run, cells were collected, counted, and calibrated to uranine recovery, then compared with the inlet concentration for the percent recovery calculation.

	% Cell recovery			% Cell reco	overy	
	Above 1e	e-4 v/v tolue	ene plume	Below 1e	-4 v/v tolue	ne plume
-	PpF1 f0	PpF1 f1	PpF1 f3	PpF1 f0	PpF1 f1	PpF1 f3
	435%	124%	96%	209%	213%	58%



**Figure 2.6.2** Plot of cell recovery for three PpF1 strains: PpF1 wild type (PpF1 f0), PpF1 single knockout strain (PpF1 f1) and PpF1 triple knockout strain (PpF1 f3), when 1e-4 v/v of toluene was fed. Recovery was plotted both when PpF1 strains were injected above and below the toluene plume.

## 2.7. 2-D Microcosm experiments: toluene analysis

Toluene quantity was measured from two 2-D microcosm experiments: one from abiotic run where no bacterial cells were introduced into the 2-D microcosm and the other from the biotic run #6 from chapter 2.6. Toluene concentration profiles from two microcosm runs were shown below in **Figure 2.7.1**. The toluene recovery from abiotic run summed up to 8.9% whereas toluene recovery from run #6 summed up to 1.1%, the difference being 7.8%. A great loss of toluene from abiotic experiments was observed, indicating that either that toluene was trapped within the microcosm or that the loss occurred during quantification process, or both.

To calculate the conversion factor of those produced daughter bacterial cells from toluene consumption over the inlet bacterial cells:

$$\# = \frac{Area_{inlet,toluene} \times V_f \times \varepsilon \times C_{toluene} \times Y_{\frac{b}{a}} \times 7.8\%}{Area_{inlet,acteria} \times V_f \times \varepsilon \times b_0} = \frac{C_{toluene} \times Y_{\frac{b}{a}} \times 7.8\%}{b_0}$$
$$= \frac{0.944 \times 9.98e - 9 \times 0.078 \frac{mol}{s}}{5.8e - 10 \frac{mol}{s}} = 1.27$$

This is number less than the maximum recovery of bacterial cells from 2-D microcosm outlet (433%). One reason could be that toluene experienced reversible absorption with the sands inside the 2-D microcosm thus provided more carbon-energy source when bacterial cells were injected into the system than 7.8% as calculated above.



**Figure 2.7.1** Toluene profiles at the microcosm outlet from an abiotic experiment and Run #6.

# 2.8. Reproducibility

Reproducibility was tested with uranine recovery from Run #1 – Run #6. In regard to the asymmetric flow pattern between the top and bottom part of the microcosm, uranine recovery was averaged for each part separately. The averaged data and corresponding graph was shown below (**Table 2.8.1** and **Figure 2.8.1**), which confirmed an acceptable fluctuation.

Furthermore, Run #5 was repeated and the reproducibility of cell recovery was tested in addition to uranine recovery. (**Table 2.8.2** and **Figure 2.8.2**) The fluctuation range was about 8% of averaged cell recovery value for PpF1 wild type, and 24% for PpF1 triple knockout strain. The higher number is primarily due to low recovery of PpF1 triple knockout strain at the outlet.

	Mean	SD	CV
Тор	83.1%	0.1412	17%
Bottom	94.8%	0.1682	18%

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 Table 2.8.1
 Averaged uranine recovery data.

Figure 2.8.1 Averaged uranine recovery.

	<b>Fable 2.8.2</b>	Averaged	PpF1 c	ell rec	covery	data.
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	Cell reco	overy (n=2)	
	Mean	SD	CV
PpF1 f0 (top)	437%	35%	8%
PpF1 f3 (bottom)	96%	24%	24%



**Figure 2.8.2** Averaged PpF1 cell recovery over 2 runs. PpF1 f0 was injected 1e-4 v/v toluene plume and PpF1 f3 below.

# **Chapter 3. Computational Simulation**

# 3.1. Introduction

To evaluate how the cell growth/death and mass transfer (chemotaxis) parameters separately affect the overall toluene consumption rate, a mathematical model was set up to quantitatively describe the transport phenomena occurring inside the 2-D microcosm. Comparison of the numerical solutions of these mathematical equations to the experimental observations will facilitate the evaluation of the impact of various parameters on bioremediation efficiency under this natural-groundwater-mimicking condition and thus the sensitivity of bioremediation efficiency to each of these parameters. Therefore, it allows us to compare the extent to which the bioremediation is dependent on the contaminant uptake step, which is related with bacterial cell growth rate, with the delivery of bacterial cells to the contaminated site. The established model could further be utilized to predict the behavior of bacterial cells and toluene with various parameter settings under non-tested conditions, and ultimately provide assistance in practical *in situ* bioremediation.

To this end, the governing equations explaining all processes including advection, dispersion, chemotaxis, bacterial cell growth/death, bacterial settling, and toluene/oxygen consumption terms were established in preparation for analysis with finite element analysis software COMSOL Multiphysics<sup>®</sup>. "Time dependent" mode was used and the computation was stopped at 19 h after initiation which was the median time point of sample collection period in experiments (18 h – 20 h). "Steady state" mode was used later to represent the condition that are closer to the real world scenario.

In this chapter, a representative simulation results were first shown matching the experimental results where the highest bacterial cell recovery were observed in experiments, and these parameters were used as a basis for subsequent simulations. To qualitatively compare the effect of chemotaxis and bacterial cell growth/death on the fate of bacterial cells as well as toluene during experiments, four combinatorial sets of simulation runs were performed where chemotaxis and bacterial cell growth/death terms were or were nor incorporated in the model. Next, for a quantitative comparison, parametric analysis was done to figure out how much sensitively the bacterial cell recovery and toluene recovery responded to each of the parameters involved in chemotaxis (chemotaxis sensitivity coefficient  $\chi_{0,eff}$  and chemotactic receptor binding constant K<sub>c</sub>) and bacterial growth/death (maximum specific growth rate  $\mu_{max}$  and half saturation constant K<sub>a</sub>). With these results, moment analysis was done with bacterial cell recovery to further study how these parameters influenced the transfer and consumption of toluene by bacteria. In regard to the previous studies that insufficient oxygen supply has well known to impede the bioremediation process by aerobic remediating bacteria, simulations were performed with incorporating or not incorporating oxygen consumption terms in the model, followed by simulations at various oxygen concentrations to study its effect. Finally, simulations were done with increased spacing between bacterial cells and toluene source, and also with increased flow rate, in which the effect of chemotaxis and bacterial growth/death under these conditions were evaluated and compared with current experimental setting.

## **3.2. Mathematical model**

A mathematical model (Equation 3.2.1 – 3.2.3) was set up to represent the transport phenomena inside the microcosm. In addition to bacterial cells (*b*) and toluene (*a*), oxygen (*o*) was also taken into consideration because insufficient oxygen availability has been observed to significantly limit the bioremediation efficiency by previous studies (54). The governing equations are listed below. These partial differential equations were solved by finite element analysis software COMSOL Multiphysics<sup>®</sup>, with the microcosm simulation configured to match the experimental setup. Parameter values were either referenced from other studies or measured and calculated in this study (**Table 3.2.1**).

$$\frac{\text{Growth /}}{\text{Accum. Dispersion Advection Consumption Decay Chemotaxis Settling}} = D_{bx} \frac{\partial^2 b}{\partial x^2} + D_{by} \frac{\partial^2 b}{\partial y^2} - V_f \frac{\partial b}{\partial x} + \left(\frac{o}{o + K_o} \frac{\mu_{max}a}{K_a + a}\right) b - k_{decay} b - \frac{\partial(V_{Chx}b)}{\partial x} - \frac{\partial(V_{Chy}b)}{\partial y} - v_{set} \frac{\partial b}{\partial y} \quad (3.2.1)$$

$$\frac{\partial a}{\partial t} = D_{ax} \frac{\partial^2 a}{\partial x^2} + D_{ay} \frac{\partial^2 a}{\partial y^2} - V_f \frac{\partial a}{\partial x} - \frac{o}{o + K_o} \frac{q_a a}{(K_a + a)} b \quad (3.2.2)$$

$$\frac{\partial o}{\partial t} = D_{ox}\frac{\partial^2 o}{\partial x^2} + D_{oy}\frac{\partial^2 o}{\partial y^2} - V_f\frac{\partial o}{\partial x} - \frac{q_o o}{(o+K_o)}\frac{a}{(K_a+a)}b$$
(3.2.3)

where b is bacterial cell concentration, a is the toluene concentration (attractant/carbon and energy source), o is the electron acceptor oxygen concentration, t is time, x is the distance longitudinally in the direction of buffer flow along the microcosm, y is the transverse distance to the x axis with x = 0 located at the center of the toluene injection zone, R is retardation factor which accounts for sorption,  $V_f$  is average interstitial velocity,  $D_{bx}$  is longitudinal dispersion coefficient for bacterial cell,  $D_{by}$  is transverse dispersion coefficient for bacterial cell,  $D_{ax}$  is longitudinal dispersion coefficient for toluene,  $D_{ay}$  is transverse dispersion coefficient for toluene,  $D_{ox}$  is longitudinal dispersion coefficient for oxygen,  $D_{oy}$  is transverse dispersion coefficient for oxygen,  $\mu_{max}$  is maximum specific growth rate of the bacterial cell on toluene,  $\mu_{max,o}$  is maximum specific growth rate of the bacterial cell on oxygen,  $K_a$  is half saturation constant for bacterial cell growth on toluene,  $K_o$  is half saturation constant for bacterial cell growth on oxygen,  $k_{decay}$  is bacterial cell decay rate,  $V_{Chx}$  is longitudinal chemotactic velocity,  $V_{Chy}$  is transverse chemotactic velocity,  $v_{set}$  is bacterial cell settling velocity due to higher gravity than buffer,  $Y_{b/a}$  is yield coefficient of the bacterial cell on toluene, the maximum toluene consumption rate  $q_a = \frac{\mu_{max}}{Y_{b/a}}$ ,  $Y_{b/o}$  is yield coefficient of the bacterial cell on oxygen, and the maximum oxygen consumption rate  $q_o = \frac{\mu_{max,o}}{Y_{b/o}}$ . (51)

The dispersion coefficients are defined by:

$$D_{ix} = \frac{D_{diff,i}}{\varepsilon} + \alpha_{ix}V_f, (i = a, b, o)$$

$$D_{diff,i} \qquad (3.2.4)$$

$$D_{iy} = \frac{D_{diff,i}}{\varepsilon} + \alpha_{iy}V_f, (i = a, b, o)$$
(3.2.5)

where i represents each species,  $D_{ix}$  is longitudinal dispersion coefficient of i,  $D_{iy}$  is transverse dispersion coefficient of i,  $D_{diff,i}$  is diffusion coefficient of i,  $\alpha_{ix}$  is longitudinal dispersivity of i, and  $\alpha_{iy}$  is transverse dispersivity of i.

The chemotactic velocity terms  $V_{Chx}$  and  $V_{Chy}$  are defined by (48):

$$V_{Chx} = \frac{2}{3} v_b \tanh\left(\frac{\chi_{0,eff}}{2v_b} \frac{K_c}{(K_c + a)^2} \frac{\partial a}{\partial x}\right)$$
(3.2.6)

$$V_{Chy} = \frac{2}{3} v_b \tanh\left(\frac{\chi_{0,eff}}{2v_b} \frac{K_c}{(K_c + a)^2} \frac{\partial a}{\partial y}\right)$$
(3.2.7)

where  $v_b$  is bacterial cell swimming speed,  $\chi_{0,eff}$  is chemotaxis sensitivity coefficient and  $K_c$  is chemotactic receptor binding constant.

The 2-D microcosm was configured such that a tank with the dimensions 95 cm (x - axis)  $\times$  13 cm (y - axis) was represented as a homogeneous porous medium with a void fraction of 0.37 (52). Flow direction was from left to right, so all inlets were located on the left side of the microcosm and outlets on the right.

Boundary conditions:

No-flux boundary conditions were used for the upper and lower boundaries of the model. The outlet boundary condition was set as  $-\mathbf{n} \cdot D_i \cdot \nabla c_i = 0$ , which means the species passing this boundary was pulled out via convective flux. Toluene with concentration of  $a_0$  and bacterial cell with concentration of  $b_0$  were injected continuously from the designated inlets of 2-D microcosm with a width of 1 cm, the width which was experimentally indicated by the color tracer uranine at the inlet once it entered the 2-D microcosm from inlet tubings.

Initial conditions (@ t=0):	
Toluene concentration:	$a = 0 \ (0 \le x \le 95 \ cm, -6.5 \ cm \le y \le 6.5 \ cm)$
Bacterial cell concentration:	$b = 0 \ (0 \le x \le 95 \ cm, -6.5 \ cm \le y \le 6.5 \ cm)$
Oxygen concentration:	$o = o_0 \ (0 \le x \le 95 \ cm, -6.5 \ cm \le y \le 6.5 \ cm)$

Toluene concentration, the sole carbon and energy source, was initially set as 0 throughout the 2-D microcosm system, and it started to enter the system from designated inlet at a concentration of  $a_0$  when the computation was initiated. Similarly, bacterial cell concentration was initially set as 0 throughout the 2-D microcosm system, and they started to enter the system from designated inlet(s) at a concentration of  $b_0$  when the computation was initiated. Oxygen concentration, the electron acceptor, was initially set as its saturated concentration  $o_0$  throughout the 2-D microcosm system, and it started to enter the system from designated inlet(s) at a concentration of  $b_0$  when the computation was initiated. Oxygen concentration, the electron acceptor, was initially set as its saturated concentration  $o_0$  throughout the 2-D microcosm system, and it started to enter the system from all inlets at its saturated concentration when the computation was initiated.

To compare the effect of chemotaxis and bacterial cell growth/death, the governing equations were modified and were listed below. Boundary conditions and initial conditions remain the same.

The governing equations when chemotaxis was not applied:

Accum. Dispersion Advection Consumption Decay Settling  

$$R\frac{\partial b}{\partial t} = D_{bx}\frac{\partial^2 b}{\partial x^2} + D_{by}\frac{\partial^2 b}{\partial y^2} - V_f\frac{\partial b}{\partial x} + \left(\frac{o}{o+K_o}\frac{\mu_{max}a}{K_a+a}\right)b - k_{decay}b - v_{set}\frac{\partial b}{\partial y}$$
(3.2.8)

$$\frac{\partial a}{\partial t} = D_{ax}\frac{\partial^2 a}{\partial x^2} + D_{ay}\frac{\partial^2 a}{\partial y^2} - V_f\frac{\partial a}{\partial x} - \frac{o}{o+K_o}\frac{q_a a}{(K_a+a)}b$$
(3.2.9)

$$\frac{\partial o}{\partial t} = D_{ox}\frac{\partial^2 o}{\partial x^2} + D_{oy}\frac{\partial^2 o}{\partial y^2} - V_f\frac{\partial o}{\partial x} - \frac{q_o o}{(o+K_o)}\frac{a}{(K_a+a)}b$$
(3.2.10)

The governing equations when bacterial cell growth/death was not applied:

Accum. Dispersion Advection Chemotaxis Settling  

$$R\frac{\partial b}{\partial t} = D_{bx}\frac{\partial^2 b}{\partial x^2} + D_{by}\frac{\partial^2 b}{\partial y^2} - V_f\frac{\partial b}{\partial x} - \frac{\partial(V_{Chx}b)}{\partial x} - \frac{\partial(V_{Chy}b)}{\partial y} - v_{set}\frac{\partial b}{\partial y}$$
(3.2.11)

$$\frac{\partial a}{\partial t} = D_{ax}\frac{\partial^2 a}{\partial x^2} + D_{ay}\frac{\partial^2 a}{\partial y^2} - V_f\frac{\partial a}{\partial x}$$
(3.2.12)

$$\frac{\partial o}{\partial t} = D_{ox}\frac{\partial^2 o}{\partial x^2} + D_{oy}\frac{\partial^2 o}{\partial y^2} - V_f\frac{\partial o}{\partial x}$$
(3.2.13)

The governing equations when bacterial cell growth/death and chemotaxis were not applied:

Accum. Dispersion Advection Settling  

$$R\frac{\partial b}{\partial t} = D_{bx}\frac{\partial^2 b}{\partial x^2} + D_{by}\frac{\partial^2 b}{\partial y^2} - V_f\frac{\partial b}{\partial x} - v_{set}\frac{\partial b}{\partial y}$$
(3.2.14)

$$\frac{\partial a}{\partial t} = D_{ax}\frac{\partial^2 a}{\partial x^2} + D_{ay}\frac{\partial^2 a}{\partial y^2} - V_f\frac{\partial a}{\partial x}$$
(3.2.15)

$$\frac{\partial o}{\partial t} = D_{ox}\frac{\partial^2 o}{\partial x^2} + D_{oy}\frac{\partial^2 o}{\partial y^2} - V_f\frac{\partial o}{\partial x}$$
(3.2.16)

To evaluate the effect of oxygen during the 2-D microcosm runs, a mathematical model without incorporating oxygen into the process was also established, wherein it was assumed that oxygen was supplied with sufficient amount and replenished immediately where it was consumed. The governing equations were listed below:

$$\frac{\text{Growth /}}{\text{Accum. Dispersion Advection Consumption Decay Chemotaxis Settling}} = D_{bx} \frac{\partial^2 b}{\partial x^2} + D_{by} \frac{\partial^2 b}{\partial y^2} - V_f \frac{\partial b}{\partial x} + \left(\frac{\mu_{max}a}{K_a + a}\right)b - k_{decay}b - \frac{\partial(V_{Chx}b)}{\partial x} - \frac{\partial(V_{Chy}b)}{\partial y} - v_{set}\frac{\partial b}{\partial y} \qquad (3.2.17)$$
$$\frac{\partial a}{\partial t} = D_{ax} \frac{\partial^2 a}{\partial x^2} + D_{ay} \frac{\partial^2 a}{\partial y^2} - V_f \frac{\partial a}{\partial x} - \frac{q_a a}{K_a + a}b \qquad (3.2.18)$$

Boundary conditions and initial conditions remained the same, except that oxygen part was excluded from the model.

The parameters used in this simulation were listed in **Table 3.2.1**. The calculations of several parameter values in this study were attached in **Appendix A8**.

Symbol	Physical meaning	Value
$a_0$	injected toluene concentration	0.94 [mol/m <sup>3</sup> ]
$b_0$	injected bacterial concentration	$5.80 \text{ e-}10 \text{ [mol/m}^3\text{]}$
<b>O</b> 0	injected oxygen concentration	$1.25 \text{ e-}3 \text{ [mol/m}^3\text{]}$
D <sub>a,bulk</sub>	bulk diffusion coefficient for toluene	$9.00 \text{ e-}10 \text{ [m}^2/\text{s]}$
D <sub>b,bulk</sub>	bulk diffusion coefficient for bacterial cell	$3.20 \text{ e-}10 \text{ [m}^2/\text{s]}$
D <sub>o,bulk</sub>	bulk diffusion coefficient for oxygen	$1.97 \text{ e-9} [\text{m}^2/\text{s}]$
$D_{ax}$	longitudinal dispersion coefficient for toluene	$1.53 \text{ e-8} [\text{m}^2/\text{s}]$
$D_{ay}$	transverse dispersion coefficient for toluene	$1.58 \text{ e-9} [\text{m}^2/\text{s}]$
$D_{bx}$	longitudinal dispersion coefficient for bacterial cell	$4.66 \text{ e-9} [\text{m}^2/\text{s}]$
$D_{by}$	transverse dispersion coefficient for bacterial cell	5.12 e-10 [m <sup>2</sup> /s]
$D_{ox}$	longitudinal dispersion coefficient for oxygen	$1.60 \text{ e-8} [\text{m}^2/\text{s}]$
$D_{oy}$	transverse dispersion coefficient for oxygen	2.35 e-9 [m <sup>2</sup> /s]
K <sub>a</sub>	half saturation constant, growth on toluene	$1.50 \text{ e-1} [\text{mol/m}^3]$
K <sub>c</sub>	chemotaxis receptor binding constant	1 [mol/m <sup>3</sup> ]
k <sub>decay</sub>	bacterial cell decay rate	1.27 e-5 [1/s]
Ko	half saturation constant, growth on oxygen	$1.25 \text{ e-}2 \text{ [mol/m}^3\text{]}$
$q_a$	maximum reaction rate of toluene	1.05 e4 [mol /mol cell s]
$q_o$	maximum reaction rate of oxygen	9.60 e4 [mol /mol cell s]
R	retardation factor	1
$U_{\text{avg}}$	apparent flow rate	5.74 e-6 [m/s]
$v_b$	bacterial cell swimming speed	4.4 e-5 [m/s]
$V_f$	average interstitial velocity	1.55 e-5 [m/s]
$v_{set}$	bacterial cell settling velocity due to gravity	6.04 e-8 [m/s]
$Y_{b/a}$	yield coefficient of the bacterial cell on toluene	9.98e-9 [mol/mol]
$\alpha_{ax}$	longitudinal dispersivity for toluene	9.41 e-4 [m]
$\alpha_{ay}$	transverse dispersivity for toluene	6.00 e-5 [m]
$\alpha_{bx}$	longitudinal dispersivity for bacterial cell	2.85 e-4 [m]
$\alpha_{by}$	transverse dispersivity for bacterial cell	1.82 e-5 [m]
$\alpha_{ox}$	longitudinal dispersivity for oxygen	9.41 e-4 [m]
$\alpha_{oy}$	transverse dispersivity for oxygen	6.00 e-5 [m]
ξ	porosity	0.37
$\mu_{max}$	maximum specific growth rate of cell on toluene	1.05 e-4 [1/s]
$\chi_{0,eff}$	chemotactic sensitivity coefficient	5 e-10 [m <sup>2</sup> /s]

 Table 3.2.1 Parameter values used in COMSOL simulation

#### **3.3. COMSOL simulation: A representative result**

In this chapter, a representative simulation result was presented, which was matched to the experimental result where highest bacterial cell recovery was observed. For this purpose, three parameters  $q_a$ ,  $q_o$ , and  $k_{decay}$  that were related with bacterial cell growth were scaled down to 0.22x of their reference values. These values were subsequently used as a basis for future simulations in this study.

Simulation was done in "time dependent" mode and was stopped at 19 h after the computation was initiated. For a comparison, "steady state" mode was also conducted and presented in parallel. Buffers carrying toluene, bacterial cells and oxygen were injected from the inlet located on the left side of the 2-D microcosm. Toluene was injected from the center inlet (y = 0 m), and bacterial cells were from the inlet located 3 cm above the toluene (y = 0.03 m). Oxygen was injected from all inlets.

A representative simulation result was shown in **Figure 3.3.1** – **3.3.3**, where the distribution of toluene, bacterial cells, and oxygen within the 2-D microcosm were shown as a function of time (0 h, 5 h, 10 h, 15 h, 18 h, 19 h, 20 h, and at steady state). Note that the sampling time during experiments were 18 h - 20 h. The concentration profiles of these species at inlet as well as at outlet were plotted as a function of time (**Figure 3.3.1** (J) and (K), **Figure 3.3.2** (J) and (K), **Figure 3.3.3** (J) and (K).

For all species (toluene, bacterial cells, and oxygen), the convective flow carried them from left to right along x direction. At the same time, dispersion caused the transport of these species in the transverse y direction. Eventually, both toluene and bacterial cells form a fan-like plume with the highest concentration along y-axis located at the center of injection inlet (assuming only advection and dispersion were involved). Initially, though the bacterial cells and toluene were distant to each other close to the inlet, they eventually would meet within the 2-D microcosm after a certain amount of time of travelling. Once the bacterial cells got exposure to toluene, two processes proceeded simultaneously: the bacterial cells sensed the gradient of toluene and the chemotaxis drove them to swim toward the center of the toluene plume where more toluene was present; at the same time, the bacterial cells started to uptake toluene which they used for survival and growth.

**Figure 3.1.1** (D) and (K) shows that toluene started to come out of the 2-D microcosm from approximately 15 h after the computation was initiated. As time went, more and more toluene came out which was shown as increased  $C_{out}/C_{in}$  value. Additionally, as toluene was consumed by more and more bacterial cells as a function of time, an increased asymmetry of toluene peaks were observed in **Figure 3.1.1** (K): plots for 15 h, 18 h, 19 h, 20 h and steady state. Less toluene were recovered from top half-section (y > 0) of the 2-D microcosm than the bottom half-section (y < 0), and this is clearly shown in the region close to the outlet.

For bacterial cells, increased concentration started to appear from approximately 15 h after the computation was initiated, as shown by combined colors of green, yellow, and red in **Figure 3.1.2** (D) - (H). Before 15 h, the color of the bacterial cell plume got slightly dimmed due to the death in the absence of carbon/energy source (toluene in this case). As bacterial cells got exposed to more and more toluene as they traveled toward the outlet, a significantly increased bacterial cell concentration was observed close to the outlets. Similar to toluene, skewed bacterial cell peaks were observed in the region close to the outlet, due to the chemotaxis as well as increased bacterial cell growth where they got exposure to higher concentration of toluene (close to y = 0 m).

For oxygen, initially oxygen were homogeneously present at its saturation concentration throughout the 2-D microcosm (**Figure 3.1.3** (A) and (J)). The bacterial cells started to grow after they got exposure to toluene, wherein the oxygen also started to be consumed. So, a region with decreased oxygen concentration started to appear from approximately 15 h after injection (**Figure 3.1.3** (D) - (H)). In **Figure 3.1.3** (K), oxygen peak started to occur approximately after 15 h, and the concentration decreased further as a function of time, due to consumption by more and more bacterial cells. The peak position located approximately at the same position as the peak for bacterial cells, indicating oxygen was consumed most quickly where most bacterial cells were present.

As shown in **Figure 3.3.1** (K), **Figure 3.3.2** (K), and **Figure 3.3.3** (K), a slight difference in the distributions of toluene, bacterial cells and oxygen at the outlet between 19 h and steady state indicated that at 19 h after the initiation of the computation, the system hasn't reached steady state yet, yet the differences were not very significant.



Figure 3.3.1 COMSOL simulation results with bacterial cell growth/death and

chemotaxis terms applied: distribution of toluene within the microcosm as a function of time. (A) 0 h; (B) 5 h; (C) 10 h; (D) 15 h; (E) 18 h; (F) 19 h; (G) 20 h after injection; (H) steady state; (I) scale bar for (A)-(H); (J) toluene concentration profile at inlet; (K) toluene concentration profile at outlet of the microcosm as a function of time.



**Figure 3.3.2** COMSOL simulation results with bacterial cell growth/death and chemotaxis terms applied: distribution of bacterial cells within the microcosm as a function of time. (A) 0 h; (B) 5 h; (C) 10 h; (D) 15 h; (E) 18 h; (F) 19 h; (G) 20 h after injection; (H) steady state; (I) scale bar for (A)-(H); (J) bacterial cell concentration profile at inlet; (K) bacterial cell concentration profile at outlet of the microcosm as a function of time.

# **Bacterial cell**



**Figure 3.3.3** COMSOL simulation results with bacterial cell growth/death and chemotaxis terms applied: distribution of **oxygen** within the microcosm as a function of time. (A) 0 h; (B) 5 h; (C) 10 h; (D) 15 h; (E) 18 h; (F) 19 h; (G) 20 h after injection; (H) steady state; (I) scale bar for (A)-(H); (J) oxygen concentration profile at inlet. (K) oxygen concentration profile at outlet of the microcosm as a function of time.

# 3.4. Comparison: cell growth/death vs. chemotaxis

During the 2-D microcosm runs, after bacterial cells and toluene met each other, both bacterial growth process and chemotaxis would lead to increased toluene consumption thus improved bioremediation efficiency. To respectively investigate the effect of each of these processes, simulation was done in four combinatorial sets: both growth/death incorporated in the mathematical model (Equation 3.2.1 - 3.2.3); chemotaxis was not incorporated (Equation 3.2.8 - 3.2.10); growth/death was not incorporated (Equation 3.2.14 - 3.2.16). The visual results of distribution of toluene, bacterial cells, and oxygen within the 2-D microcosm at 19 h were shown in **Figure 3.4.1**, and the concentration profiles of each species at the outlet for each of four sets were plotted in **Figure 3.4.2**.

In **Figure 3.4.1** (A1), the same as presented in chapter 3.3, decreased amount of toluene distribution in the region close to the 2-D microcosm outlet (top half-section) was observed where both chemotaxis and bacterial cell growth/death were applied. When chemotaxis was not applied (**Figure 3.4.1** (A3)), toluene distribution didn't show much difference from **Figure 3.4.1** (A1), indication insignificance of chemotaxis process. However, when bacterial cell growth/death was not applied (**Figure 3.4.1** (A2) and (A4)), higher concentration of toluene was observed in the region close to the outlet. This indicated that the low concentration of the toluene in the region close to the 2-D microcosm outlet was primarily due to cell growth/death terms that were incorporated in the mathematical model rather than the chemotaxis terms.

Similarly, the analysis of bacterial cell distribution in four sets of experiments (**Figure 3.4.1** (B1) - (B4)) confirmed the same results from the analysis of toluene above. The significantly increased bacterial cell concentration in the region close to the 2-D

microcosm outlet were mainly due to the bacterial cell growth/death terms in the mathematical model, and the chemotaxis term barely generated observable difference.

During 2-D microcosm runs, oxygen was solely consumed by bacterial cells, so the distribution of oxygen was similar to that of bacterial cell, however, in inverse fashion (**Figure 3.4.1** (C1) – (C4)). Again, the decreased oxygen distribution in the region close to the 2-D microcosm outlet aroused primarily from the bacterial growth/death terms.

The concentration profile of each species at the 2-D microcosm outlet for the four combinatorial sets of simulations confirmed the conclusion from above visual observation. In **Figure 3.4.2** (A), the higher two toluene peaks were for the computation where bacterial growth/death was not applied whereas the lower two peaks were for that where bacterial growth/death was applied. However, the peaks basically overlapped to each other when chemotaxis was applied and was not applied (**Figure 3.4.2** (A) thick grey line *vs.* black dash line, black dot line *vs.* thin grey line). Lower toluene peaks were due to the consumption by more bacterial cells in that region (**Figure 3.4.2** (B)). When bacterial cell growth/death was not applied, oxygen concentration remained at the same concentration value because it was not consumed by bacterial cells (**Figure 3.4.2** (C)), and when bacterial cell growth/death was applied, a decrease in oxygen concentration was observed where bacterial cell peaks were present. Moreover, whether the chemotaxis was applied or not did not lead to observable difference in the oxygen concentration profile at the 2-D microcosm outlet.

In summary, the simulation with four combinatorial sets where chemotaxis and bacterial growth/death terms were or were not applied suggest that, the latter played a greater role in the fate of toluene, bacterial cell and oxygen, and the incorporation of bacterial

growth/death terms significantly increase the number of bacterial cells within the microcosm leading to the significant decrease in toluene recovery from the 2-D microcosm outlet.



**Figure 3.4.1** Simulation results: effect of bacterial cell growth/death and chemotaxis on the distribution of toluene, bacterial cells, and oxygen distribution. Images were captured 19 h after injection. (A) Toluene distribution within 2-D microcosm: (A1) with growth/death and chemotaxis, (A2) with chemotaxis only, (A3) with growth/death only, (A4) without growth/death and chemotaxis; (B) Bacterial cell distribution within 2-D microcosm: (B1) with growth/death and chemotaxis, (B2) with chemotaxis only, (B3) with growth/death only, (B4) without growth/death and chemotaxis; (C) Oxygen distribution within 2-D microcosm: (C1) with growth/death and chemotaxis, (C2) with chemotaxis only, (C3) with growth/death only, (C4) without growth/death and chemotaxis.



**Figure 3.4.2** Simulation results: effect of bacterial cell growth/death and chemotaxis on the distribution of toluene, bacterial cells, and oxygen distribution at the outlet of 2-D microcosm. Each concentration profile was captured at 19 h after injection. (A) Toluene; (B) Bacterial cell; (C) Oxygen. (thick grey line: with growth/death and chemotaxis; black dash line: with chemotaxis only; black dot line: with cell growth only; think grey line: without growth/death and chemotaxis)

# 3.5. Parametric study

Chapter 3.4 closed with the conclusion that bacterial growth/death had greater effect on toluene consumption during microcosm runs than chemotaxis, by comparing the conditions where each of the above two terms was entirely taken out from the mathematical model. In this chapter, in order to quantitatively test how the parameters concerning these two processes affect the overall remediation efficiency, simulation work by varying these parameter values over a range were conducted, and how the fate of each species got affected was studied. The parameters to vary during the simulations were: chemotaxis sensitivity coefficient  $\chi_{0,eff}$  and chemotactic receptor binding constant  $K_c$  for chemotaxis process; maximum growth rate  $\mu_{max}$  and half saturation constant  $K_a$  for cell growth/death process. Each of the abovementioned parameters were varied over its reference values that were set in chapter 3.3 by a factor ranging from 0.1x to 10x. First, COMSOL computations were done in "time dependent" mode to represent current experimental setup. The concentration of bacterial cells and toluene at the 2-D microcosm outlet were plotted, and the area under the peaks was summed up to quantify them. Bacterial cell and toluene recovery were calculated by dividing the overall bacterial cell or toluene harvested at the outlet by the amount injected at the inlet  $(\frac{\sum C_{out}}{C_{int}})$ . The same sets of computations were also performed with "stationary mode" which was a closer mimic of natural groundwater system where the steady state would probably have evolved over the long course of time after the release of the contaminant to the site. Moment analysis was then performed for the bacterial cell distribution at the 2-D microcosm outlet to further investigate how each parameter influenced the fate of bacterial cells and ultimately the toluene cleanup and bioremediation efficiency.

## 3.5.1 Sensitivity analysis of simulation results with current experimental setup

**Figure 3.5.1.1** shows a tornado chart where the sensitivity of bacterial cell recovery (A) and toluene recovery (B) to each of bacterial cell growth/death related parameters and chemotaxis related parameters was respectively drawn. Each parameter value was varied over the range from -50% to 200% of its reference value (which matched to current experimental setup in chapter 3.3). It was apparently shown that the both bacterial cell recovery and toluene recovery showed greater sensitivity to bacterial growth related parameters  $\mu_{max}$  and  $K_a$  than chemotaxis related parameters  $\chi_{0,eff}$  and  $K_c$ .  $\mu_{max}$  and  $\chi_{0,eff}$  were positively correlated with bacterial cell recovery while  $K_a$  and  $K_c$  were negatively correlated. Since higher bacterial recovery indicates more consumption of toluene,  $\mu_{max}$  and  $\chi_{0,eff}$  were negatively correlated. This justified the use of bacterial cell recovery as the indicator of bioremediation efficiency during 2-D microcosm experiments in chapter 2.

The four parameters were further varied over a larger range from 0.1x to 10x (except for  $\mu_{max}$ ), and the corresponding bacterial cell recovery and toluene recovery were calculated and listed in **Table 3.5.1.1**. Recovery data for 5x and 10x of reference value of  $\mu_{max}$  were not available because COMSOL failed to converge using these parameter values, probably because the rapid increase in bacterial cell numbers or decrease in toluene/oxygen concentration ran out of the tolerable range of COMSOL.  $\mu_{max}$ , represents the growth rate of bacterial cells, so with 0.1x of reference value of  $\mu_{max}$ , it increased up to 803%.  $K_a$  represents the affinity between toluene and bacterial cells in Monod equation characterizing bacterial cell growth upon the substrate (toluene in this case), and bacterial growth rate is inversely proportional to  $K_a$  (Equation 3.2.1). 0.1x reference value of  $K_a$  led to 791% of bacterial cell recovery and 10 x of reference value

of  $K_a$  led to 19.5% of bacterial cell recovery. These were in consistent with the fact that, regardless of the mass transfer barrier, increasing  $\mu_{max}$  and decreasing  $K_a$  led to faster cell growth cultured as in homogeneous liquid media while decreasing  $\mu_{max}$  and increasing  $K_a$  led to slower growth.



Figure 3.5.1.1 Tornado chart for sensitivity analysis of bacterial cell recovery and toluene recovery to growth and chemotaxis parameters, with 19-h sample.

**Table 3.5.1.1** Parametric study with bacterial cell recovery and toluene recovery, with 19-h sample.

Bacterial cell recovery (x100%), 19-h sample				Tolue	ene recove	ry (x100	‰), 19-h sa	ample	
Fold #	$\mu_{max}$	K <sub>a</sub>	X0,eff	Kc	Fold #	μ <sub>max</sub>	Ka	X0,eff	Kc
0.1x	0.149	7.91	4.28	4.74	0.1x	0.885	0.108	0.606	0.586
0.5x	0.608	7.76	4.31	4.53	0.5x	0.895	0.287	0.603	0.595
1x	4.45	4.45	4.45	4.45	1x	0.600	0.600	0.600	0.600
2x	8.03*	1.20	4.57	4.32	2x	0.088*	0.857	0.592	0.602
5x	N/A	0.318	4.57	4.30	5x	N/A	0.932	0.569	0.605
10x	N/A	0.195	5.47	4.29	10x	N/A	0.944	0.532	0.606
*recovery for 1.2x of reference value of $\mu_{max}$			*recovery	for 1.2x o	freference	value of $\mu$	max		

In natural groundwater system, once the contaminant was released, the plume develops over time and the steady state would have reached over a long time. To mimic this condition, the mathematical models were solved additionally in "steady state" mode and sensitivity analysis was performed in the same way as done in "time-dependent" mode above. **Figure 3.5.1.2** showed the Tornado chart where parameters were varied over the range from -50% to 200%, and **Table 3.5.1.2** showed the sensitivity of bacterial cell recovery and toluene recovery over a larger range from 0.1x to 10x of reference value of each parameter. Similar to what was observed in "time-dependent" mode, they showed greater sensitivity to growth related parameters  $\mu_{max}$  and  $K_a$ , and the correlation trend with four parameters were the same as well.



**Figure 3.5.1.2** Tornado chart for sensitivity analysis of bacterial cell recovery and toluene recovery to growth and chemotaxis parameters at steady state. (note: recovery values at 120% of  $\mu_{max}$  instead of those at 200% were plotted)

Bacterial cell recovery (x100%), steady state				Tolue	ene recove	ery (x100%	%), steady	state	
Fold #	μ <sub>max</sub>	K <sub>a</sub>	X0,eff	Kc	Fold #	μ <sub>max</sub>	K <sub>a</sub>	<b>X</b> 0,eff	Kc
0.1x	0.169	N/A	5.04	5.29	0.1x	0.995	N/A	0.584	0.560
0.5x	0.700	7.81	5.08	5.19	0.5x	0.945	0.278	0.580	0.571
1x	5.13	5.13	5.13	5.13	1x	5.13	5.13	5.13	5.13
2x	7.38*	1.44	5.23	5.09	2x	0.358*	0.884	0.567	0.580
5x	N/A	0.354	5.54	5.05	5x	N/A	0.978	0.541	0.583
10x	N/A	0.209	6.01	5.04	10x	N/A	0.991	0.499	0.583
*recovery	*recovery for 1.2x of reference value of $\mu_{max}$			*recovery	for 1.2x o	freference	value of $\mu$	max	

**Table 3.5.1.2** Parametric study with bacterial cell recovery and toluene recovery, at steady state.

To calculate the sensitivity, bacterial cell recovery were plotted over each of the varied parameters, and the curves were fitted with equations of either polynomial or exponential decay functions whichever gave the least sum of squares (**Figure 3.5.1.3, Appendix A10**). The sensitivity was defined by the slope of the tangential line of the fitted curve (the reference point "Fold # = 1" indicates the parameter values used in current experimental setup), which were listed in **Figure 3.5.1.3** (E). The bacterial cell recovery was more sensitive to bacterial cell growth (10.6 for  $\mu_{max}$  and -4.82 for  $K_a$ ) and less to chemotaxis (0.104 for  $\chi_{0,eff}$  and -0.0958 for  $K_c$ ). Positive sign indicated positive correlation and negative sign indicated negative correlation.

The sensitivity value also showed a change at difference Fold #. For  $\mu_{max}$ , there was no big change within the range of 0.5x and 1.2x, and similarly, it was almost linear relationship for  $\chi_{0,eff}$ . For  $K_a$  and  $K_c$ , the slope was very steep in the range of  $0.1x \sim 2x$ , then showed almost no change when it increased for up to 10x. It inferred that increasing the affinity of toluene could be desirable to increase the bioremediation efficiency, either by increasing the affinity with toluene uptake receptors or that with chemotactic receptors on the surface of the bacterial cell.



**Figure 3.5.1.3** Fitted curves for sensitivity calculation (reference point: x=1). The table below listed the calculated sensitivity for growth and chemotaxis parameters.

## 3.5.2 Moment analysis of simulation results with current experimental setup

To investigate how each above-mentioned parameter influenced the behavior of bacterial cells when they were transported within the 2-D microcosm, the bacterial cell concentration was plotted along y-axis at 2-D microcosm outlet at each value of the respective parameter, as drawn in **Figure 3.5.2.1**. The first, second, and third moment of the peaks were calculated (**Appendix A4**), which respectively represents the center of mass, the spread, and the skewness of the bacterial cell peaks. These three moments were affected by each of the parameters in different fashion and the eventual appearance of the peaks would result from comprehensive function of them. Note that toluene was injected from the inlet located at y = 0. So toluene concentration was highest at y = 0 and gradually decreased in both ±y directions. Bacterial cells were injected from the inlet located at y = 0.03 m.

After a certain time after injection, the bacterial cells got exposure to toluene, and subsequently sensed the toluene gradient and swam toward higher concentration of toluene via chemotaxis mechanism. This would lead to the downward movement (movement toward y = 0) of the center of mass of bacterial cells (first moment), and the greater the chemotaxis (increasing  $\chi_{0,eff}$  and decreasing  $K_c$ ), the higher degree of downward setting. As the bacterial cells closer to the center of toluene plume would experience higher toluene gradient (**Figure 3.3.1**), they would move faster than the bacterial cells distant to the center of the toluene plume, as a result, this would lead to a positively skewed bacterial cell distribution peak (third moment), and subsequently, broader peaks (second moment).

The influence of  $\mu_{max}$  and  $K_a$  are more complicated. After the bacterial cells got exposure to toluene, they would start to grow. The original bacterial cell distribution was
a symmetric peak centered at y = 0.03 m. However, the bacterial cells below this line would get exposed to more toluene and grew faster than those cells located above this line. This faster growth of the bacterial cells at the bottom would always lead to the downward movement of the center of mass of bacterial cells, while the final peak would appear as a sum of residual bacterial cells (less closer to y = 0) and newly generated bacterial cells (more closer to y = 0). The growth would also contribute to broaden and to positively skew the peak as it would pull up the tail of the originally symmetric bacterial cell peak. However, the growth of bacterial cells upon exposure to toluene would increase the peak height and this would result in a narrowed, as well as less skewed peak. In a word, the final shape of the bacterial peaks would result from the comprehensive interaction of the four parameters, in particular, would depend on which one would exert a dominant effect.

In regard to the effect of  $\chi_{0,eff}$  (Figure 3.5.2.1 (C) and (E)), with its increase, the center of mass of bacterial peak moved downward (toward y = 0 direction where toluene concentration was highest) a little bit but was negligible. However, as this lead to exposure to more toluene, a slight increase in bacterial cell number (peak area) could be observed. Additionally, a slightly increasing broadness of the peak as well as slightly increasing positive skewness was observed. These were inconsistence with above analysis. In regard to the effect of  $K_c$  (Figure 3.5.2.1 (D) and (E)), as chemotaxis got weakened with its increase, the trend was the opposite of that of  $\chi_{0,eff}$ .

In regard to the effect of  $\mu_{max}$  (Figure 3.5.2.1 (A) and (E)), with its value increased up to 1x, the center of mass moved downward a bit. The width of the peak decreased more and more up to 1x of  $\mu_{max}$  but suddenly increased at 1.2x. This was due to the faster growth of the bacterial cells upon exposure to higher concentration of toluene closer to y = 0.

The same trend was observed for the skewness of the peak for the same reason, except that the turning point occurred at 0.5x of its reference value. The effect of  $K_a$  (Figure 3.5.2.1 (C) and (E)) was opposite of that of  $\mu_{max}$ . A constantly downward movement of center of mass was observed, and similar to what was observed for  $\mu_{max}$  effect, complicated responses in broadness as well as skewness of the peak were observed, due to the interplay of the different processes. Besides, a more drastic change in bacterial cell number (peak area) due to bacterial cell growth/death related parameters in comparison to chemotaxis related parameters could be observed.



Figure 3.5.2.1 Concentration profiles of bacterial cells at the outlet at various parameter values.

				Mome	nt analysis (l	Bacteria	al cell)			
			m1	m2	m3			m1	m2	m3
		Fold #	ŷ (cm)	$\sigma^2(cm^2)$	γ		Fold #	ŷ (cm)	$\sigma^2(cm^2)$	γ
-		0.1x	-2.98	0.697	2.42E-08		0.1x	-3.00 <sup>&amp;</sup>	0.779 <sup>&amp;</sup>	4.50E-07 <sup>&amp;</sup>
eatl		0.5x	-2.99	0.680	1.34E-07		0.5x	-3.00	0.657	3.30E-07
p/q		1x	-2.99	0.578	1.88E-07	V	1x	-2.99	0.578	1.88E-07
wt	$\mu_{max}$	2x	-3.00*	0.979*	5.38E-07*	<b>N</b> a	2x	-2.99	0.670	2.13E-07
2C		5x	N/A	N/A	N/A		5x	-2.98	0.773	1.24E-07
Ŭ		10x	N/A	N/A	N/A		10x	-2.98	0.773	1.24E-07
		0.1x	-2.99	0.578	1.88E-07		0.1x	-2.99	0.574	1.93E-07
ixis		0.5x	-2.99	0.578	1.87E-07		0.5x	-2.99	0.577	1.91E-07
lota		1x	-2.99	0.578	1.88E-07	K	1x	-2.99	0.578	1.88E-07
nem	<b>X</b> 0,eff	2x	-2.99	0.578	1.93E-07	R <sub>c</sub>	2x	-2.99	0.578	1.87E-07
CP		5x	-2.99	0.579	2.09E-07		5x	-2.99	0.578	1.85E-07
		10x	-2.99	0.579	2.09E-07		10x	-2.99	0.578	1.85E-07

**Table 3.5.2.1** Moment analysis.  $\overline{y}$  was listed in reference to the injection position.

\*recovery for 1.2x of reference value of  $\mu_{max}$ 

<sup>&</sup>recovery for 0.2x of reference value of K<sub>a</sub>

# 3.6 Effect of oxygen supply

For bioremediation with aerobic bacteria, it has been well studied that limited oxygen supply significantly impedes the bioremediation process (53, 54). To elucidate the role of oxygen in current 2-D microcosm experiments, mathematical models incorporating and not incorporating oxygen consumption terms were set up, as shown in **Equation** 3.2.17 – 3.2.18. Simulation was done in "steady state" mode, and the visual 2-D results as well as the plots of toluene, bacterial cells, and oxygen at the outlet of 2-D microcosm were also shown (**Figure 3.6.1** and **3.6.2**). By observation, there was no apparent difference in toluene and bacterial cell distribution when oxygen consumption were or were not applied (**Figure 3.6.1** (A) and (B) *vs.* **Figure 3.6.2** (A) and (B), **Figure 3.6.1** (F) *vs.* **Figure 3.6.2** (F)), while decreased oxygen concentration in the region close to the outlet were observed in **Figure 3.6.1** (C) which was not the case when oxygen was not being consumed in **Figure 3.6.3**, it can be seen that incorporation of oxygen into the model didn't have any effect on the pattern, demonstrating that oxygen was not limiting the growth of the bacterial cells or the consumption of the toluene by the bacterial cells.



**Figure 3.6.1** With  $O_2$  incorporated in the model. Distribution of toluene (A), bacterial cell (B), and oxygen (C) within the 2-D microcosm at steady state. (D) is the scale bar for (A) and (C), and (E) is the scale bar for (B). Concentration profile of toluene, bacterial cell, and oxygen at the outlet were plotted over y-axis in (F).



**Figure 3.6.2** Without  $O_2$  incorporated in the model. Distribution of toluene (A), bacterial cell (B), and oxygen (C) within the 2-D microcosm at steady state. (D) is the scale bar for (A) and (C), and (E) is the scale bar for (B). Concentration profile of toluene, bacterial cell, and oxygen at the outlet were plotted over y-axis in (F).



**Figure 3.6.3** Comparison of toluene and bacterial cell recovery when oxygen was and wasn't incorporated in the mathematical model.

Next, simulations were done with varied oxygen concentrations, from 0.1x for up to 2.8x (56, 57) of the oxygen concentration used in current experimental setup. Bacterial cell as well as toluene recovery was plotted over the varied oxygen concentrations. It was clearly shown that at 0.1x of reference oxygen concentration, bacterial cell growth and toluene cleanup were significantly limited; at 0.5x of reference oxygen concentration, bacterial cell growth and toluene cleanup were moderately affected; from 1x to up to 2.8x of reference oxygen concentration, bacterial cell growth and toluene cleanup didn't change much. This again confirmed that, the oxygen supply was not limiting the bioremediation efficiency under current experimental setup, and toluene was the sole bacterial cell growth limiting as well as toluene cleanup limiting factor.



Figure 3.6.4 Effect of oxygen concentration on toluene and bacterial cell recovery.

## 3.7. Effect of spacing between bacterial cell and toluene

To study the behavior of bacterial cells more distant to the contaminated site than current experimental setting, the injection inlet for the bacterial cells were moved up 1 cm resulting in the distance of 4 cm between the bacterial cell and toluene injection inlet. COMOSL simulations were performed the same way as in Chapter 3.3, and the results were shown in **Figure** 3.7.1 (3 cm spacing) and 3.7.2 (4 cm spacing). With increased spacing, no significant decrease (**Figure 3.7.1** (A) and (F)) in toluene concentration in the region close to 2-D microcosm outlet was observed as in the closer spacing in **Figure 3.7.2** (A) and (F). Consequently, no significant cell growth or decrease in oxygen concentration (**Figure 3.7.2** (B), (C) and (F)) in the region close to the outlet was observed as compared with in closer spacing (**Figure 3.7.1** (B), (C) and (F)).

Similar to the sensitivity analysis with 3 cm spacing, a tornado chart was drawn to study the sensitivity of bacterial cell as well as toluene recovery to the four parameters related with bacterial cell growth/death and chemotaxis (**Figure 3.7.3** and **Table 3.7.1**). The overall bacterial recovery was lower and toluene recovery was higher, at this distant region, due to less exposure of the bacterial cells to toluene throughout the 2-D microcosm runs. The sensitivity was still higher for bacterial cell growth/death process than the chemotaxis process. The quantitative analysis of the sensitivity also showed the same trend as in closer spacing (**Figure 3.7.4** and **Table 3.7.2**)



**Figure 3.7.1** With 3 cm spacing between bacterial cell and toluene (experimental setup). Distribution of toluene (A), bacterial cell (B), and oxygen (C) within the 2-D microcosm at steady state. (D) is the scale bar for (A) and (C), and (E) is the scale bar for (B). Concentration profile of toluene, bacterial cell, and oxygen at the outlet were plotted over y-axis in (F).



**Figure 3.7.2** With 4 cm spacing between bacterial cell and toluene. Distribution of toluene (A), bacterial cell (B), and oxygen (C) within the 2-D microcosm at steady state. (D) is the scale bar for (A) and (C), and (E) is the scale bar for (B). Concentration profile of toluene, bacterial cell, and oxygen at the outlet were plotted over y-axis in (F).



**Figure 3.7.3** Tornado chart for sensitivity analysis of bacterial cell recovery (A) and toluene recovery (B) to growth and chemotaxis parameters at steady state, with increased spacing between bacterial cells and toluene.

Table 3.7.1	Parametric	study wit	h bacterial	cell	recovery	and	toluene	recovery,	with
increased sp	acing betwe	en bacteri	al cells and	l tolu	ene.				

Bacterial cell recovery (x100%), steady state				Toluene recovery (x100%), steady state					
Fold#	μ <sub>max</sub>	K <sub>a</sub>	X0,eff	Kc	Fold#	μ <sub>max</sub>	K <sub>a</sub>	X0,eff	Kc
0.1x	0.138	5.148*	0.561	0.599	0.1x	0.999	0.600*	0.964	0.961
0.5x	0.222	1.766	0.565	0.577	0.5x	0.991	0.872	0.964	0.963
1x	0.570	0.570	0.570	0.570	1x	0.963	0.963	0.963	0.963
2x	7.538	0.262	0.581	0.566	2x	0.429	0.988	0.963	0.964
5x	N/A	0.165	0.613	0.563	5x	N/A	0.996	0.960	0.964
10x	N/A	0.143	0.670	0.561	10x	N/A	0.998	0.956	0.964
*recovery for 0.2x of reference value of $K_a$				*recovery	for 0.2x c	of reference	value of K	- a	



Figure 3.7.4 Fitted curves for sensitivity calculation at the reference point (x=1) with simulation with increased spacing between bacterial cells and toluene. The table below listed the calculated sensitivity for growth and chemotaxis parameters with increased spacing between bacterial cells and toluene, as well as those from current experimental setup for comparison.

#### 3.8. Effect of flow rate

In this chapter, the effect of groundwater flow rate on the bacterial behavior and toluene cleanup process was studied. As compared the flow rate used in the experimental setup 1.55 e-5 m/s, an elevated flow rate of 1.76 e-4 m/s was tested (45, 46). A comparison was shown in **Figure 3.8.1 and 3.8.2**. The decrease in toluene concentration, bacterial cell growth, and decrease in oxygen concentration in the region close to 2-D microcosm outlet were no longer observable at high flow rate. Though higher flow rate was beneficial in terms of promoting the transfer of species perpendicular to the flow rate by increasing the dispersion (where i is one of the species toluene, bacterial cell or oxygen,  $D_{iy} = \alpha_{iy} \times V_f + \frac{D_{i,eff}}{\varepsilon}$ ), the increased flow rate dramatically decreased the residence time of the species by carrying them away even faster through the convective flow. As a result, the bacterial cells had decreased time period for them either to sense the toluene gradient to give chemotactic response or to uptake toluene to reproduce themselves. The calculated dispersion coefficient for toluene, bacterial cells, and oxygen were listed in **Table 3.8.1**.

Sensitivity analysis was performed the same way in chapter 3.5, and at higher flow rate, the bacterial cell growth/death related parameters still played a greater role than chemotaxis in terms of toluene cleanup rate and bioremediation efficiency. (**Figure 3.8.3**, **Figure 3.8.4**, and **Table 3.8.2**)



**Figure 3.8.1** Simulation result at  $V_f = 1.55 \text{ e-5 m/s}$  (experimental setup). Distribution of toluene (A), bacterial cell (B), and oxygen (C) within the 2-D microcosm at steady state. (D) is the scale bar for (A) and (C), and (E) is the scale bar for (B). Concentration profile of toluene, bacterial cell, and oxygen at the outlet were plotted over y-axis in (F).



**Figure 3.8.2** Simulation result at  $V_f = 1.76$  e-4 m/s. Distribution of toluene (A), bacterial cell (B), and oxygen (C) within the 2-D microcosm at steady state. (D) is the scale bar for (A) and (C), and (E) is the scale bar for (B). Concentration profile of toluene, bacterial cell, and oxygen at the outlet were plotted over y-axis in (F).

	V <sub>f</sub> =1.55e-5 m/s	V <sub>f,hi</sub> =1.76e-4 m/s
D <sub>ay</sub>	3.36E-09	1.30E-08
$\mathbf{D_{by}}$	1.15E-09	4.07E-09
Doy	6.25E-09	1.59E-08

Table 3.8.1 Dispersion coefficient of toluene, bacterial cell, and oxygen at low and high flow rate.



**Figure 3.8.3** Tornado chart for sensitivity analysis of bacterial cell recovery and toluene to growth and chemotaxis parameters at steady state, with higher flow rate.

Bacterial cell recovery (x100%), steady state					Toluene recovery (x100%), steady state				
Fold#	$\mu_{max}$	K <sub>a</sub>	X0,eff	Kc	Fold#	$\mu_{max}$	Ka	X0,eff	K <sub>c</sub>
0.1x	0.838	0.982*	0.880	0.883	0.1x	1.000	0.990*	0.997	0.997
0.5x	0.856	0.914	0.880	0.881	0.5x	0.999	0.995	0.997	0.997
1x	0.880	0.880	0.880	0.880	1x	0.997	0.997	0.997	0.997
2x	0.932	0.859	0.881	0.880	2x	0.981	0.999	0.997	0.997
5x	1.13	0.844	0.883	0.880	5x	0.939	1.000	0.997	0.997
10x	1.79	0.839	0.886	0.880	10x	0.939	1.000	0.997	0.997
*recovery	*recovery for 1.2x of reference value of K <sub>a</sub>					for 0.2x c	of reference	value of K	-a

**Table 3.8.2** Parametric study with bacterial cell recovery and toluene recovery, with higher flow rate.



**Figure 3.8.4** Fitted curves for sensitivity calculation at the reference point (x=1) with simulation with higher flow rate. The table below listed the calculated sensitivity for growth and chemotaxis parameters with higher flow rate, as well as those from current experimental setup for comparison.

# **Chapter 4. Conclusions and Recommendations**

The transport of microorganisms through the saturated porous matrix of soil is critical to the successful implementation of bioremediation in polluted groundwater systems. Motile bacteria that are self-propelled are able to swim independently of the groundwater flow and thereby enhance their accessibility to the hydrocarbon pollutants which they chemically transform and use as carbon and energy sources. Access to the hydrocarbons, thus provides a competitive advantage and increases the growth rate of the motile bacterial population, which ultimately led to improved bioremediation efficiency. In this study, a 2-D rectangular-shaped microcosm packed with quartz sand was used to study the transport and population growth of bacteria within a saturated model aquifer system as well as the resulting toluene cleanup efficiency. A model system comprising *Pseudomonas putida* F1 (PpF1) strains and toluene, to which PpF1 is chemotactic to and with which PpF1 could utilize as their carbon and energy source for survival and growth, was employed. Species of *Pseudomonas putida F1*, either PpF1 wild type or PpF1 mutants (PpF1 ( $\Delta todX$ ) or PpF1 ( $\Delta todX \Delta cym D \Delta F1 fadL$ )) that lacked a mechanism to transport toluene across the outer cell membrane, were injected above or below the toluene. The ability to take up toluene into the cell resulted in significantly greater population growth of the PpF1 wild type as compared to the mutants. The established mathematical model also confirmed the sensitiveness of the toluene degradation efficiency to bacterial growth related parameters which was directly correlated with toluene uptake capability, regardless of the presence of mass transfer barrier. And this sensitiveness was reserved under different conditions such as in a region more distant to toluene source and with an increased flow rate. This suggests that, in addition to mechanisms that enhance the delivery of the degrading agents to the contaminated site, transport membrane proteins of bacteria can also play a key role in bioremediation enhancement. Moreover, it suggests the potential of engineering bacteria toward higher contaminant permeability for enhanced bioremediation efficiencies. Overall, the results indicated that the coupling between transport of motile bacteria and population growth facilitated by uptake of toluene leads to a greater abundance of bacteria in the vicinity of the plume that will aid biodegradation in groundwater systems that are not naturally well-mixed. Furthermore, it suggested the potential to engineer toluene-degrading bacteria toward greater toluene permeability for enhanced bioremediation efficiency.

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# Appendices

# A1. Uranine quantification

Uranine as a conservative tracer was injected from the inlet together with cells to trace the flow pattern in the microcosm. Uranine was quantified by measuring its absorbance with a plate reader. As samples from the outlet ports were subjected to filtration prior to measurement, the PpF1 cells wouldn't interfere uranine quantification at this wavelength. Uranine showed an absorbance peak at wavelength of 490 nm, so this wavelength was used for quantifying uranine. Uranine solution was serially diluted and the calibration curve was drawn as below by plotting the absorbance value at 490 nm versus the uranine concentration.



**Figure A1.1** Adsorption spectrum of uranine. Uranine has an absorption peak at ~490 nm.



Figure A1.2 Calibration curve of uranine, measured with absorption at 490 nm.

Uranine (mM)	Avr., A <sub>490</sub>	SD, A <sub>490</sub>	CV, A <sub>490</sub>
0	0	0	
0.001	0.015	0.001	5%
0.0025	0.079	0.000	0%
0.005	0.154	0.001	1%
0.0075	0.234	0.003	1%
0.01	0.311	0.001	0%
0.025	0.771	0.002	0%
0.05	1.488	0.021	1%

Table A1.1 Calibration curve of uranine measured with adsorption at 490 nm.

# A2. Cell enumeration

For enumeration, cells suspended in the sample were collected by centrifugation, stained with a fluorescent dye, confirmed of the fluorescent property by fluorimeter, and then cell numbers were counted with a flow cytometer.

### A2.1. Cell staining

Cells were stained with a fluorescent dye in order to remove the possible signal interference from sand and debris *etc.* when counting with flow cytometer. The dye to stain the cells is FM® 4-64 Dye (N-(3-Triethylammoniumpropyl)-4-(6-(4-(Diethylamino) Phenyl) Hexatrienyl) Pyridinium Dibromide) (Life Technologies, CAT# T3166). FM® 4-64 Dye is a lipophilic styryl compound which is nontoxic to cells and virtually nonfluorescent in aqueous media. It is believed to insert into the outer leaflet of the surface membrane where it becomes intensely fluorescent. This method of membrane labeling has been used to selectively visualize plasma membrane in cultured bacteria (55, 56).

Cells were stained according to the following the procedure. 500 uL of sample containing cells was pelleted by centrifugation at 10,000 xg for 5 min, then supernatant was discarded and cells were suspended in1 mL of filtered M9 media via vortexing and collected by centrifugation again. This washing step was performed twice. Then cells were suspended in 1 mL of filtered M9 media again and 1 uL 5 mg/mL of FM<sup>®</sup> 4-64 Dye stock solution was added and mixed well together. The solution was covered by foil and put at room temperature for 10 min for staining. Then washing was performed as the same procedure as above and stained cells were finally suspended in at a final volume of 0.5 mL M9 media for further analysis with fluorimeter and flow cytometer.



Figure A2.2.1 Excitation and emission spectrum of cells stained with FM4-64. Ex/Em for stained cells is  $\sim$  500 nm/650 nm.

### A2.2. Fluorimeter analysis

A fluorimeter is a device used to measure parameters of fluorescence. The intensity and wavelength distribution of the emission spectrum of the sample can be measured after excitation by a certain spectrum of light. These parameters are used to identify the presence and the amount of specific molecules in a medium.

PpF1 cells stained with FM® 4-64 (57, 58) were reported to be excited at 506 nm and emitted at 750 nm. In reference to this, to optimize the excitation and emission wavelength in current setting of the experiment, the stained cell suspension was first subjected to emission scan with excitation wavelength of 500 nm, then with the emission wavelength that exhibited maximum fluorescence thereof, excitation scan was done thereafter. Slit number was set as 5 for both excitation and emission scans. 2 mL of cell suspension was used for measurement and cell concentration was about 0.5 OD<sub>590</sub> as measured before dying with FM® 4-64.

The result shows that the stained cells exhibit maximum excitation wavelength at around 500 nm and maximum emission wavelength at around 650 nm (**Figure A2.2.1**). These values fall approximately within the analysis range of the current laser configuration of the flow cytometer, which is integrated with excitation wavelength of 488 nm and emission filter of 610/20 nm at the detector position FL3.

#### A2.3. Flow cytometer analysis

Flow cytometry is a process of performing measurements on particles including cells that are in liquid suspension. It is a technology that simultaneously measures and analyzes multiple characteristics of particles as they pass through a beam of light, such as relative size, internal complexity and fluorescence intensity. Typically particles or cells from 0.2 - 50 micrometers in size are suitable for flow cytometry analysis. A flow cytometer is composed of three main subsystems: fluidics, optics, and electronics. The fluidics subsystem transports the particles of interest to the interrogation point where they interact with the excitation sources. The optics subsystem provides the excitation sources and the components to collect light signals and route them to the appropriate detectors.

The electronic subsystem converts light signals to equivalent electronic signals. When particles flow through the laser beam, light scattering occurs in two directions: the forward scatter light which gives the relative particle size information, and the side scatter light which gives the information on particle granularity or internal complexity. If the particles contain fluorochromes, either by staining or having been engineered to express fluorescent molecules in the case of cells, this particle population can also be identified according to the type of the fluorochrome that they have.

A threshold is the lowest signal intensity value an event can have for it to be recorded by

the cytometer. The signal pulse must exceed the level set on the threshold to be recorded as an event on any other channel. When choosing the appropriate threshold value, debris and undesired events should be eliminated without inadvertently eliminating relevant events. If this is the first time a particular experiment is performed, it might not be clear which events are the correct ones, so they must be identified. Once the particles have been identified, the threshold should be set low enough to ensure the entire population is captured. The ideal placement of the threshold is somewhere between the particles of interest and the noise floor.

The BD Accuri<sup>TM</sup> C6 flow cytometer has a default threshold setting of FSC-H as 80,000, which has been optimized for mammalian cell analysis. As PpF1 is typically 1 um in length, much smaller than mammalian cells, the FSC-H threshold must be further lowered for the analysis in this study, or the majority of cells would be excluded from the recorded events. Additionally, the stained cells provide an additional threshold option of FL3-H, to separate them from nonfluorescent noises.

During the optimization process of flow cytometer parameters, both stained and unstained cells were prepared. Cells were cultured to logarithmic phase in LB media under optimal condition (30 °C, 150 rpm, 9 h culture). Unstained cells were prepared by direct centrifugation of cell culture at 10,000 xg for 5 min, then supernatant was discarded and cells were suspended in fresh filtered analysis media and collected by centrifugation again. This washing step was performed twice. Then cell concentration was adjusted to  $OD_{590}$  value of 1, and this will be defined as 1x OD cell concentration in the following statements for convenience. Accordingly, 0.1x OD cell concentration means cell concentration is where the absorbance value is 0.1 at 590 nm. For stained cell samples, the same staining procedure was performed as mentioned above in the "staining

cell" section.

IX WIS ITIEUIA	l				
	Threshold	10k	20k	30k	
	FSC-H	23.282	37.717	63.715	
Size	mean	,		,- ••	
	FSC-H modian	11,259	26,636	43,539	
	meulan				
	FL3-H	000	504	4 005	
FM64-4	mean	200	531	1,085	
Signal	FL3-H	166	236	197	
	median	100	230	407	
Unstaned ce	lls				
	Threshold	10k	20k	30k	
	FSC-H	57 718	64 042	71 843	
Size	mean	01,110	01,012	11,010	
	FSC-H	49,599	55,428	62,423	
	median				
	FL3-H	0.07	040	045	
FM64-4	mean	307	310	315	
Signal	FL3-H	200	202	207	
	median	290	295	291	
Stained cells	6				
	Threshold	10k	20k	30k	
	FSC-H	60 136	58 991	66 795	
Size	mean	00,100	00,001	00,700	
	FSC-H	52,008	51,008	58,665	
	median	-		•	
	FL3-H				
FM64-4	mean	26,642	26,994	28,056	
Signal	FL3-H	00000	04554	05000	
U	median	23903	24554	25639	

 Table A2.3.1 Optimization of FSC-H threshold for cell counting. No cells (M9 media only), unstained cells and stained cells were counted with various FSC-H thresholds.

 1x M9 media

For each analysis, 300 uL of sample containing cells was injected and the washing step with filtered DW for 2 min was performed between every measurement. Back-flushing and unclogging were done from time to time.

Firstly, FSC-H threshold was optimized (Table A2.3.1, Figure A2.3.1). FSC-H threshold

was optimized with 1x cell concentration of unstained cells and stained cells. M9 media was also analyzed as background analysis. Optimization was done with single threshold of FSC-H, and values of 50k, 30k, 20k, and 10k were tested.

With the increasing threshold of FSC-H, mean as well as median size of the detected particles showed approximately increasing trend for both unstained and stained cell samples. This is not surprising, as higher FSC-H threshold would exclude more events including the particles of interest while excluding the false positives in the sample. Data for M9 media only with FSC-H threshold of 10k, however, shows higher FSC-H and FL3-H mean values as well as median values than the sample with stained cells. This is probably due to the residual dyes from the previously run experiments for stained cells with various FSC-H thresholds. Stained cells exhibited higher FL3-H values compared with unstained cell as well as M9 media, as FL3-H recorded events by the fluorescence signal generated by the particles of interest. Change of FSC-H threshold hardly affected the FL3-H value. It could be noticed that M9 media also gave a good number of events reading, necessitating the inclusion of another threshold for the removal of background noise. Based on the comparison result of different FSC-H threshold, 10k was chosen for cell enumeration.

Secondly, FL3-H threshold was optimized. With FSC-H threshold value set as aboveoptimized value of 10k, further optimization of FL3-H threshold was performed with 0.1x cell concentration of stained and unstained cells. Plotting event number versus FL3-H, the majority of events in stained cell sample fell in FL3-H higher than 1k, while less than 1k for unstained cell sample and M9 media. (**Figure A2.3.2**)



**Figure A2.3.1** Optimization of FSC-H threshold for cell counting. M9, unstained cells and stained cells were counted with various FSC-H thresholds. In the vertical direction from top to bottom, FSC-H thresholds are 10 k, 20 k and 30 k in turn.



**Figure 6.2.3.2** Optimization of FL3-H threshold. Stained cells, unstained cells and M9 samples were counted with FSC-H threshold of 10k, and cell counts were plotted over FL3-H value.



**Figure A2.3.3** Cell counting of serially diluted stained cell samples. Cell counts of 1x, 0.1x and 0.01x stained cell samples were plotted over FL3-H value.

**Table A2.3.2** Event counting of M9 with various parameters. Double thresholds - FSC-H of 10 k and FL3-H of 1 k - gave negligible recordings.

	Thres		
Sample	FSC-H	FL3-H	# Events
M9	10k	None	21077
M9	10k	1k	6
M9	9k	1k	67
M9	8k	1k	149
M9	7k	1k	379
M9	5k	1k	1676
M9	10k	900	76
M9	10k	800	314

Event number versus FL3-H was also plotted for serially diluted stained cell samples. (**Figure 6.2.3.3**) A small number of the recordings below FL3-H value of 1000 is supposed to be background noises.

With further dilution, less events were recorded at the region where FL3-H was higher than 1k. Regarding previous result, FL3-H threshold of 1k was selected in addition to FSC-H threshold of 10k to remove the noises from unstained cells and debris *etc*. Thirdly, background from M9 was checked. To check background from M9 media, flow cytometer analysis was done with buffer only with double thresholds, FSC-H threshold of 1k.

M9 gave events number of 6 with double threshold set as above, which is almost negligible comparing with the event number recorded for stained cells. (**Table A2.3.2**) Fourthly, the calibration curve was drawn with the above parameters. With optimized double thresholds, FSC-H threshold of 10k and FL3-H threshold of 1k, flow cytometer analysis was done with serially diluted stained cell samples and the recorded events were plotted versus the cell dilution factor. It showed a refined linear correlation within the range of 0.01x to 0.1x cell concentration. At lower cell concentration range, it showed linear correlation with a different slope. (**Figure A2.3.4**)



**Figure. A2.3.4** Calibration curve of cell counting with flow cytometer. Double thresholds - FSC-H of 10 k and FL3-H of 1 k - were used.
#### A3. Toluene quantification by GC-MS

Toluene fraction was quantified from 2 mL sample aliquots by liquid-liquid extraction with 0.7 mL of cyclohexane containing 9.42 mg/L ethylbenzene as internal standard. Aqueous sample and the organic solvent were mixed together in a sealed glass vial, and then, after shaking for 1 h at room temperature at 100 rpm, the organic solvent phase was collected for further GC-MS analysis. GC-MS analysis was done with Shimadzu GCMS-QP2010 Plus (Kyodo, Japan) equipped with a DB-5MS column with dimension of 0.5 µm film thickness, 0.25 i.d., 30 m length from Agilent (Santa Clara, CA, United States). Sample injection was on splitless mode and the flow rate of the carrier gas helium was 1 mL min–1. The oven temperature was 40 °C for 1 min, then ramped first at a rate of 20 °C min–1to 180 °C and then at a rate of 30 °C to 300 °C where it was held for 1 min. The MS was operated at 280 °C in the SIM scan mode for the masses 91.00 and 98.00. Washing step with pure extraction solvent was done with the same temperature program between each sample run to remove any residual contaminant peaks.

For toluene calibration curve, 2 mL of calibration samples, which are microcosm buffer containing various concentrations of toluene, were incubated with 0.7 mL cyclohexane containing ethylbenzene as described above, and then the solvent phase were subjected to GC-MS analysis after 1 h of shaking. A small background peak appeared as noise with the sample where organic solvent was incubated with buffer only. The standard deviation was determined and the limit of detection of this established quantification protocol was determined as approximately three times of this standard deviation value. The noise information and calibration curve are shown below. The dynamic range is toluene concentrations of 1e-8 (v/v) to 1e-5 (v/v), so samples were subjected to dilution when toluene concentration in them run above this range.

Table A3.1 GC-MS noise peak information (n=3).				
	Avr.	SD	CV	
Buffer	2.88e4	412	1%	

**Table A3.2** Toluene calibration curve from GC-MS (n=3), noise peak area has been deducted from original value.

Toluene (v/v)	Avr.	SD	CV
1.00E-08	4.65e3	1.32e3	28%
1.00E-07	2.38e4	2.04e3	9%
1.00E-06	2.94e5	8.52e3	3%
1.00E-05	5.49e6	3.55e5	6%



Figure A3.1 Toluene calibration curve by GC-MS analysis.

#### A4. Moment analysis

Moment analysis was done to analyze the vertical movement of the analyte.

The first moment, namely the mean value  $\mu$ , represents the center of mass of the analyte and was determined from the following equation:

 $\mathbf{m}_1 = \mu = \hat{\mathbf{y}} = \Sigma(C_i * y_i) / \Sigma C_i$ 

The second moment, namely the variance  $\sigma^2$ , represents the spread of analyte and was determined from the following equation:

$$\mathbf{m}_2 = \sigma^2 = \Sigma C_i * (\mathbf{y}_i - \hat{\mathbf{y}})^2 / \Sigma C_i$$

The third moment, namely the skewness of the peak, represents the preferable movement of the analyte:

 $m_3 = \gamma = \Sigma C_i * (y_i - \hat{y})^3 / \Sigma C_i$ 

Where  $y_i$  is the outlet number,  $C_i$  is the analyte concentration percentage as compared with the inlet.

## A5. Gaussian fitting

Gussian fitting was done with "Dynamic 3-parameter Gaussian fitting" module in SigmaPlot software, the equation being:

$$f(x) = ae^{-\frac{(x-b)^2}{2c^2}}$$

where "b" denotes the center of the peak and "c" equals to " $\sigma$ " which denotes the peak breadth.

## A6. Medium and buffer recipes (47, 59)

## • M9 medium (1 L)

Na<sub>2</sub>HPO<sub>4</sub> 2.7 g, KH<sub>2</sub>PO<sub>4</sub> 3 g, NaCl 0.5 g, NH<sub>4</sub>Cl 1 g, MgSO<sub>4</sub> 0.1 mM, CaCl<sub>2</sub> 0.1 mM, pH 7.0 (adjust with 10 M NaOH)

## • LR plate (1 L)

#### • LR liquid media (1 L)

 $KH_2PO_4 24g, NaOH 1g, (NH_4)_2SO_4 1.675g, MgSO_4 \bullet H_2O \quad 0.3 \quad g, FeSO_4 \bullet 7H_2O \quad 3 \quad mg,$  concentrated  $H_2PO_4 \quad 10 \ uL$ 

# A7. 2-D microcosm experiments: scheme, image, analyte concentration profile, and data analysis

2-D microcosm experiments were conducted by simultaneous injection of two of three PpF1 strains into the microcosm in each run, which makes total of 6 runs. The scheme of each 2-D microcosm experiment, along with the actual image taken at the end and the concentration profiles of the analyte, are shown in **Figure A7.1**. Gaussian fitting was done for symmetric peaks and moment analysis was done for asymmetric peaks, as shown in **Table A7.2**.

Table A7.1 Three types of PpF1 strains and genotype

Strain label	Strain type	Strain genotype
PpF1 f0	PpF1 wild type	PpF1 wild type
PpF1 f1	PpF1 single knockout	$PpF1 (\Delta todX)$
PpF1 f3	PpF1 triple knockout	PpF1 ( <i>∆todX∆cymD∆F1fadL</i> )



**Figure A7.1** 2-D Microcosm experiments with PpF1 f0, PpF1 f1 and PpF1 f3: scheme, images and concentration profiles of uranine and PpF1 cells at the outlet (continued on next page).



**Figure A7.2** 2-D Microcosm experiments with PpF1 f0, PpF1 f1 and PpF1 f3: scheme, images and concentration profiles of uranine and PpF1 cells at the outlet (continued from last page).

			Uranin	ie			Cell	
	Inject	Mean	Breadth	Skewness		Mean	Breadth	Skewness
	position	ŷ	$\sigma^2$	Υ	_	ŷ	$\sigma^2$	Ŷ
Dup #1	Тор	-0.41	1.09	-0.25		-0.28	0.46	-0.25
Kull #1	Bottom	-0.34	2.10	0.30		-0.97	0.56	0.30
Dup #2	Тор	-0.16	1.72	0.83		-0.45	2.81	0.83
$\operatorname{Kull} \# Z$	Bottom	0.11	2.29	1.60		-1.21	1.54	1.60
Dup #2	Тор	0.90	1.95	-0.20		-0.81	0.77	-0.20
Kull #3	Bottom	0.12	2.43	0.76	_	-1.06	0.93	0.76
Dup #4	Тор	0.15	0.93	0.14		-0.83	1.66	0.14
Kull #4	Bottom	-0.07	2.14	0.98		-0.61	1.58	0.98
Dup #5	Тор	-0.49	1.64	-0.17		-0.06	0.63	-0.17
Kull #3	Bottom	-0.20	1.89	0.80		-0.36	1.22	0.80
Dup #6	Тор	0.27	2.34	0.31		-1.26	1.08	0.31
Kull #0	Bottom	-0.53	3.02	1.57		-0.92	1.44	1.57
Dave #51	Тор	0.81	1.59	-0.20		0.11	0.74	-0.20
Run #5'	Bottom	0.17	2.55	0.28		-0.66	0.89	0.28

**Table A7.2** List of peak parameters from Gaussian fitting and moment analysis for uranine and PpF1 strains in 2-D microcosm run  $\#1 \sim \#5$  (#5' is repeat run of #5). *Italic numbers* are from Gaussian fitting and others from moment analysis.

## A8. COMSOL parameter calculations

List of given parameters:

$$\varepsilon = 0.37 (62)$$

$$V_{f} = \frac{l_{microcosm}}{traveling time} = \frac{0.95 m}{17 \times 3600s} = 1.55e - 5 \frac{m}{s} (\text{this study})$$

$$U_{avg} = \varepsilon \times V_{f} = 0.37 \times 1.55e - 5 \frac{m}{s} = 5.74e - 6 \frac{m}{s}$$

$$MW_{toluene} = 92.14 \ g/mol$$

$$MW_{oxygen} = 32.00 \ g/mol$$

$$D_{a,bulk} = 9.00e - 10 \frac{m^{2}}{s}$$

$$D_{b,bulk} = 3.20e - 10 \frac{m^{2}}{s} (48)$$

$$D_{o,bulk} = 1.97e - 9 \frac{m^{2}}{s}$$

$$D_{ax,ref} = 1.95e - 8 \frac{m^{2}}{s} (38)$$

$$D_{ay,ref} = 1.85e - 9 \frac{m^{2}}{s} (38)$$

$$\alpha_{ay} = 6.00e - 5 m (5)$$

$$V_{f,ref} = 2.00e - 5 \frac{m}{s} (38)$$

$$Y_{b/t} = 1.28 \frac{g \ cell}{g \ toluene}$$

$$q_{e} = \frac{\mu_{m,o}}{Y_{b/o}} = 2.60e - 4 \frac{g \ cell}{g \ oxygen \cdot s}$$

1. Bacterial setting velocity:  $v_{set}$ 

$$v_{set} = \frac{l_{set}}{t} = \frac{1 \ cm}{17 \ h \times 3600 \ s} \times \varepsilon = 6.04e - 8 \ cm/s$$

2. Bacterial cell volume:  $V_b$ 

Assuming average bacterial cell size: length  $l_b = 0.5 \ \mu m$ , diameter  $d_b = 0.5 \ \mu m$ 

The volume of single cell:

$$V_b = \frac{\pi}{4} d_b^2 l_b = \frac{\pi}{4} (0.5 \,\mu m)^2 \times (0.5 \,\mu m) = 9.82 \text{e-}20 \,m^3$$

Assuming wet cell density is  $1 \text{ g/}cm^3$ , and bacterial cell is approximately composed

of 80% of water (61), the dry cell density:

$$\rho_b = 20\% \times 1 \frac{g}{cm^3} = 2.00e5 \frac{g}{m^3}$$

So, mass of dry single cell:

$$m_b = \rho_b \times V_b = (2.00 \text{e}5\frac{g}{m^3}) \times (9.82\text{e}-20 \text{ }m^3) = 1.96\text{e}-14 \text{ g}$$

So, molecular weight of single dry cell:

$$MW_b = m_b \times N_A = 1.96e-14 \text{ g} \times 6.02e23 = 1.18e10 \frac{g}{mole}$$

3. Yield coefficient on toluene:  $Y_{b/a}$  (51)

$$Y_{b/a} = 1.28 \frac{g \, cell}{g \, toluene} = \frac{\frac{1.28 \, g}{MW_b}}{\frac{1 \, g}{MW_toluene}} = \frac{\frac{2.55 \, g}{1.18e10 \frac{g}{mol}}}{\frac{1 \, g}{92.14 \frac{g}{mol}}} = 9.98e-9 \frac{mole \, cell}{mole \, toluene}$$

4. Maximum oxygen consumption rate:  $q_e$ 

$$q_e = \frac{\mu_{m,o}}{\frac{Y_b}{o}} = 2.6e - 4\frac{g \text{ oxygen}}{g \text{ cell} \cdot s} = \frac{\frac{2.60e - 4g}{MW_o}}{\frac{1g}{MW_b} \cdot s} = \frac{\frac{2.6e - 4g}{32.00\frac{g}{mole}}}{\frac{1g}{1.18e10\frac{g}{mol}} \cdot s} = 9.60e4$$

 $\frac{mole \ oxygen}{mole \ cell \cdot s}$ 

5. Toluene longitudinal dispersivity:  $\alpha_{ax}$ 

Since

$$D_{ax,ref} = \alpha_{ax} \times V_{f,ref} + \frac{D_{a,eff,ref}}{\varepsilon_{ref}}$$

$$D_{ay,ref} = \alpha_{ay} \times V_{f,ref} + \frac{D_{a,eff,ref}}{\varepsilon_{ref}}$$

So,

$$\alpha_{ax} = \frac{D_{ax,ref} - D_{ay,ref} + \alpha_{ay} \times V_{f,ref}}{V_{f,ref}}$$
$$= \frac{1.95e - 8\frac{m^2}{s} - 1.85e - 9\frac{m^2}{s} + 6.00e - 5m \times 2.00e - 5\frac{m}{s}}{2.00e - 5\frac{m}{s}}$$
$$= 9.41e - 4m$$

6. Toluene longitudinal dispersion coefficient:  $D_{ax}$ 

According to Millington-Quirk equation tells the relation between porosity  $\varepsilon$  and tortuosity  $\tau$  (62):

$$\tau = \varepsilon^{-\frac{1}{3}}$$
  
Since  
$$\frac{D_{toluene,eff}}{\varepsilon} = \frac{D_{toluene,bulk}}{\tau} (63)$$
  
So,

$$\frac{D_{a,eff}}{\varepsilon} = \frac{D_{a,bulk}}{\tau} = \frac{D_{a,bulk}}{\varepsilon^{-\frac{1}{3}}} = \frac{9.00e - 10\frac{m^2}{s}}{0.37^{-\frac{1}{3}}} = 6.46e - 10\frac{m^2}{s}$$

So,

$$D_{ax} = \alpha_{ax} \times V_f + \frac{D_{toluene,eff}}{\varepsilon} = 9.41e - 4m \times 1.55e - 5\frac{m}{s} + 6.46e - 10\frac{m^2}{s}$$
$$= 1.53e - 8\frac{m^2}{s}$$

7. Toluene transverse dispersion coefficient:  $D_{ay}$ 

$$D_{ay} = \alpha_{ay} \times V_f + \frac{D_{a,eff}}{\varepsilon} = 6.00e - 5 m \times 1.55e - 5 \frac{m}{s} + 6.46e - 10 \frac{m^2}{s}$$
$$= 1.58e - 9 \frac{m^2}{s}$$

8. Bacterial cell transverse dispersion coefficient:  $D_{by}$ 

According to Einstein relation:

$$D_T = \frac{\sigma^2}{2t}$$

So,

$$D_{by} = \frac{\sigma_b^2}{2t} = \frac{7.00e - 5 m^2}{2 \times 19 \times 3600s} = 5.12e - 10 \frac{m^2}{s}$$

9. Bacterial cell transverse dispersivity:  $\alpha_{by}$ 

$$\frac{D_{b,eff}}{\varepsilon} = \frac{D_{b,bulk}}{\tau} = \frac{D_{b,bulk}}{\varepsilon^{-\frac{1}{3}}} = \frac{3.20e - 10 \frac{m^2}{s}}{0.37^{-\frac{1}{3}}} = 2.30e - 10 \frac{m^2}{s}$$

Since

$$D_{by} = \alpha_{by} \times V_f + \frac{D_{b,eff}}{\varepsilon}$$

So,

$$\alpha_{by} = \frac{1}{V_f} \left( D_{by} - \frac{D_{b,eff}}{\varepsilon} \right) = \frac{1}{1.55e - 5\frac{m}{s}} \left( 5.12e - 10\frac{m^2}{s} - 2.30e - \frac{10m^2}{s} \right)$$
$$= 1.82e - 5m$$

10. Bacterial cell longitudinal dispersivity:  $\alpha_{bx}$ 

Since

$$\frac{\alpha_{by}}{\alpha_{bx}} = \frac{\alpha_{ay}}{\alpha_{ax}} = \frac{6.00e - 5m}{9.41e - 4m} = 6.38e - 2$$

So,

$$\alpha_{bx} = \frac{\alpha_{by}}{6.38e - 2} = \frac{1.82e - 5m}{6.38e - 2} = 2.85e - 4m$$

11. Bacterial cell longitudinal dispersion coefficient:  $D_{bx}$ 

$$D_{bx} = \alpha_{bx} \times V_f + \frac{D_{b,eff}}{\varepsilon} = 2.85e - 4 \ m \times 1.55e - 5\frac{m}{s} + 2.30e - 10\frac{m^2}{s}$$
$$= 4.66e - 9 \ \frac{m^2}{s}$$

12. Oxygen longitudinal dispersion coefficient:  $D_{ox}$ 

$$\frac{D_{o,eff}}{\varepsilon} = \frac{D_{o,bulk}}{\tau} = \frac{D_{o,bulk}}{\varepsilon^{-\frac{1}{3}}} = \frac{1.97e - 9\frac{m^2}{s}}{0.37^{-\frac{1}{3}}} = 1.41e - 9\frac{m^2}{s}$$
$$D_{ox} = \alpha_{ox} \times V_f + \frac{D_{o,eff}}{\varepsilon} = \alpha_{ax} \times V_f + \frac{D_{o,eff}}{\varepsilon}$$
$$= 9.41e - 4\ m \times 1.55e - 5\frac{m}{s} + 1.41e - 9\frac{m^2}{s} = 1.60e - 8\frac{m^2}{s}$$

13. Oxygen transverse dispersion coefficient:  $D_{oy}$ 

$$\frac{D_{o,eff}}{\varepsilon} = \frac{D_{o,bulk}}{\tau} = \frac{D_{o,bulk}}{\varepsilon^{-\frac{1}{3}}} = \frac{1.97e - 9\frac{m^2}{s}}{0.37^{-\frac{1}{3}}} = 1.41e - 9\frac{m^2}{s}$$
$$D_{oy} = \alpha_{oy} \times V_f + \frac{D_{o,eff}}{\varepsilon} = \alpha_{ay} \times V_f + \frac{D_{o,eff}}{\varepsilon}$$
$$= 6.00e - 5\ m \times 1.55e - 5\frac{m}{s} + 1.41e - 9\frac{m^2}{s} = 2.35e - 9\frac{m^2}{s}$$

## A9 COMSOL setting window capture

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Figure A9.1 COMSOL parameter setting.

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Figure A9.2 COMSOL Mesh setting.

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**Figure A9.3** COMSOL setting for toluene (1).

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**Figure A9.4** COMSOL setting for toluene (2).

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Figure A9.5 COMSOL setting for bacterial cell (1).

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Figure A9.6 COMSOL setting for bacterial cell (2).

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Figure A9.7 COMSOL setting for oxygen (1).

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V ← Q.2.Zmk.mph (root)     Component 1 (comp1)     Component 1 (comp1)     Comfinitions     A Geometry 1     Comfort 1     Component 1 (comp1)     Comfort 1     Component 1     Compone	Label:       Reactions 1         Domain Selection	Add Ph     Graphi     Proper     Settin       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q       Q     Q     Q     Q     Q
		709 MB   4787 MB

Figure A9.8 COMSOL setting for oxygen (2).

# A10 Calculation of sensitivity of bacterial cell recovery to bacterial cell growth and chemotaxis parameters

Below: "f" denotes bacterial cell recovery, and "x" denotes Fold # of reference value of corresponding parameters

1) Experimental setup (3 cm spacing & Low flow rate)

 $\mu_{max}$ 

Fitting line:  $f = -2.0053+3.6865*x+3.4490*x^2$ 

Slope = 
$$\frac{df}{dx}$$
 = 3.6865 + 2 \* 3.4490 \* x

 $K_a$ 

Fitting line:  $f = 13.0888 \exp(-1.0005 x)$ 

Slope = 
$$\frac{df}{dx}$$
 = (-1.0005) \* 13.0888 \* exp(-1.0005 \* x)

 $\chi_{0,eff}$ 

Fitting line:  $f = 5.0256 + 0.1056 \times x - 0.0008 \times x^2$ Slope  $= \frac{df}{dx} = 0.1056 + 2 \times (-0.0008) \times x$ 

 $K_c$ 

```
Fitting line: f = 5.0497 + 0.2642 \exp(-1.1827 x)
Slope = \frac{df}{dx} = (-1.1827) * 0.2642 * \exp(-1.1827 * x)
```

2) With increased spacing (4 cm)

 $\mu_{max}$ 

Fitting line: 
$$f = 0.0176 + 1.4324 \times -3.0143 \times -2+2.0889 \times -3$$
  
Slope  $= \frac{df}{dx} = 1.4324 + 2 \times (-3.0143) \times x + 3 \times 2.0889 \times x^2$ 

 $K_a$ 

Fitting line: 
$$f = 0.2130 + 10.4237 \exp(-3.7488 * x)$$
  
Slope  $= \frac{df}{dx} = (-3.7488) * 10.4237 * 10.4237 * \exp(-3.7488 * x)$ 

## $\chi_{0,eff}$

Fitting line: 
$$f = 0.5602 + 0.0101 \times +8.8854E - 005 \times ^2$$
  
Slope  $= \frac{df}{dx} = 0.0101 + 2 \times (8.8854E - 005) \times x$ 

## $K_c$

Fitting line: 
$$f = 0.5608 + (0.0096/x) - (0.0006/x^2)$$
  
Slope  $= \frac{df}{dx} = -0.0096/x^2 - (-2) * 0.0006/x^3$ 

## 3) High flow rate

#### $\mu_{max}$

Fitting line: 
$$f = 0.8325 + 0.0480 \times -0.0003 \times -2 + 0.0005 \times -3$$
  
Slope  $= \frac{df}{dx} = 0.0480 - 2 \times 0.0003 \times x + 3 \times 0.0005 \times -2$ 

## $K_a$

Fitting line:  $f = 0.8392 + (0.0385/x) - (0.0018/x^2)$ Slope  $= \frac{df}{dx} = -0.0385/x^2 - (-2) * 0.0018/x^3$ 

## $\chi_{0,eff}$

Fitting line: 
$$f = 0.8797 + 0.0006 * x + 4.3732E - 007 * x^2$$
  
Slope  $= \frac{df}{dx} = 0.0006 + 2 * (4.3732E - 007) * x$ 

 $K_c$ 

•

Fitting line: 
$$f = 0.8797 + (0.0006/x) - (2.9422E - 005/x^2)$$
  
Slope  $= \frac{df}{dx} = (-1) * 0.0006/x^2 - (-2) * (2.9422E - 005)/x^3$